## STEEL JOIST REPORT

## For Open Web Steel Joist 18K3SP x 22'-0"

Project: Demo
Location:
Job num.: T001

Mark: J-1

## Submitted by:

$W(D L)=66.000$
$W(L L)=316.000$ $W(D L+L L)=382.000$


## LEGEND:

O Top Bridging
O Bottom Bridging
O Bottom UpLift Bridging (Both End First V)

## Joist name: 18K3SP

Quantity top chord members=13
Quantity bottom chord Members=12
Quantity end members=2
Quantity aux. web members=2
Quantity interior web members=20
Quantity vertical web members=0
Quantity reinforcement web members=0
Total members $=49$
Total nodes=27
Quantity top chord node=14
Quantity Bottom chord node=13
Modulus of elasticity of steel=29,000 ksi(200,000 MPa)

Control effective depth $=17.220$ in $(437.388 \mathrm{~mm})$

JoistLab v6 by All View System (www.allviewsystem.com )

18K3SP x 21'-8" (OVL 22'-0")
MARK ~ J-1
MAKE ~ ONE

## Project: Demo

Job Number: T001


R7/8"diam. xCut Total Lenght=3'-0 11/16"
Outside Arc=2 5/16" Long; Inside Radius=2 1/2" diam. Interior Angle=IA=126.826 Deg.
Make $=\mathrm{ONE}$


R7/8"diam. xCut Total Lenght=3'-1 1/8"
Outside Arco $=25 / 16^{\prime \prime}$ Long; Inside Radius=2 1/2" diam. Interior Angle $=1 \mathrm{~A}=126.826 \mathrm{Deg}$ Make $=$ ONE

2 - V1 - R1/2 x $3^{\prime}-3$ 3/8" ( $A=1^{\prime}-415 / 16$ "; B=1'-7 5/16"; R=1 3/16")
6 - V2 - R5/8 x 3'-3 7/16" (A=1'-4 15/16"; B=1'-7 3/8"; R=1 1/16")
2 - V3 - R3/4 x 3'-3 1/2" (A=1'-4 15/16"; B=1'-7 7/16"; R= 15/16")

## Bill of Material

## Project Name: Demo Job Number: T001

Joist Name: 18K3SP x 22'-0" Joist Mark: J-1 Quantity: 1

| Mark | Qty | Designation | Type | Lenght | Reinforcement | Type | Lenght | Weight | Fy | Remark |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CHORDS |  |  |  |  |  |  |  |  |  |  |
| TC | 2 | L1 1/2x1 1/2x1/8 | 2 Anges | 22'-0" | N/A | N/A | N/A | 54.120Lbs | 50ksi | Top Chord |
| BC | 2 | L1 1/4x1 1/4x1/8 | 2 Anges | 17'-8" | N/A | N/A | N/A | 35.687Lbs | 50ksi | Bottom Chord |
| WEB MEMBERS |  |  |  |  |  |  |  |  |  |  |
| LE | 1 | R7/8 | Rod | 3'0 11/16" | N/A | N/A | N/A | 6.242Lbs | 50ksi | Left end member |
| RE | 1 | R7/8 | Rod | 2'-10 9/16" | N/A | N/A | N/A | 41.051Lbs | 50ksi | Right end member |
| LA | 1 | R1/2 | Rod | 1'-9 15/16" | N/A | N/A | N/A | 1.219Lbs | 50ksi | Left aux. member |
| RA | 1 | R1/2 | Rod | 1'-9 15/16" | N/A | N/A | N/A | 1.219Lbs | 50ksi | Right aux. member |
| V WEB MEMBERS |  |  |  |  |  |  |  |  |  |  |
| V1 | 2 | R1/2 | Rod/Rod | 3'-3 3/8" | none/none | N/A | N/A | 4.375Lbs | 50ksi | A=1'-4 15/16";B=1'-7 5/16";R=1 3/16" |
| V2 | 6 | R5/8 | Rod/Rod | 3'-37/16" | none/none | N/A | N/A | 20.540Lbs | 50ksi | A=1'-4 15/16"; $\mathrm{B}=1{ }^{\prime}-7$ 3/8";R=1 1/16" |
| V3 | 2 | R3/4 | Rod/Rod | 3'-3 1/2" | none/none | N/A | N/A | 9.875Lbs | 50ksi | $A=1{ }^{\prime}-415 / 16{ }^{\prime \prime} ; B=1^{\prime}-77 / 16{ }^{\prime \prime} ; R=15 / 16{ }^{\prime \prime}$ |
| BEARING |  |  |  |  |  |  |  |  |  |  |
| LB | 2 | L2x2x5/16 | Angles | $6^{\prime \prime}$ | N/A | N/A | N/A | 3.920Lbs | 50ksi | Left seat bearing |
| RB | 2 | L2x2x5/16 | Angles | $6^{\prime \prime}$ | N/A | N/A | N/A | 3.920Lbs | 50ksi | Right seat bearing |
|  |  |  |  |  |  |  |  |  |  |  |
| TOTAL | 22 |  |  |  |  |  |  | 182.17 Lbs |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| ADDITIONAL INFO. |  |  |  |  |  |  |  |  |  |  |
| Surface area |  | 43.35 sf |  |  |  |  |  |  |  |  |
| Primer | $1 \mathrm{gal}(\mathrm{s})$ |  |  |  |  |  |  |  |  | Std. Red Oxide Primer |
| Design Weight |  | 6.261Lbs/tt. |  |  |  |  |  |  |  | Not seat bering included |
| Real Weight |  | 8.280Lbs/tt. |  |  |  |  |  |  |  | With seat bering |
| Real Weight |  | 7.924Lbs/tt. |  |  |  |  |  |  |  | Not seat bering included |
| SJl Weight |  | $6.400 \mathrm{Lbs} / \mathrm{ft}$. |  |  |  |  |  |  |  | Not seat bering included |

## Project: Demo

Job Number: T001


R1/2 $\times$ Total Lenght of Rod --> Cut=3'-3 3/8"(2,2 )
V1

## Project: Demo

Job Number: T001

Int. Diameter=1 1/16"
Weld all.=19.181 kips
2Total weld Lenght. $=10 \quad 5 / 16$ " Weld Size (right) $=1 / 8^{\prime \prime}$ Weld Lenght (right) $=53 / 16^{\prime \prime}$

Weld Size (left)= $1 / 8$ " Weld Lenght (left) $=53 / 16$ "

## Eccentricity

Tang $=0.53 ; x=0.75 ; y=1.41$


R5/8 x Total Lenght of Rod --> Cut=3'-3 7/16"(2,2 )
V2

## Project: Demo

Job Number: T001

Weld Size (left)= $1 / 8$ " Weld Lenght (left) $=53 / 16$ "

## Eccentricity

Tang $=0.53 ; x=0.75 ; y=1.41$

Weld Size=1/8
Design Lenght=1'-7 15/16'
Weld all. $=5.877 \mathrm{kips}$ Weld Lenght. $=3$ 3/16"

| B.E = Both end <br> Member Name | Mem | I-J | Designation[Reinf.] |  | Lenght | Weld Information |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Top chord left first end panel (Lep1) | 1 | 1-2 | L1 1/2x1 1/2x1/8[NA] | $\urcorner\ulcorner$ | 1'-4" | N/A |
| Top chord left second end panel (Lep2) | 2 | 2-3 | L1 1/2x1 1/2x1/8[NA] | าг | 2'-0" | N/A |
| Top chord interior panel | 3 | 3-4 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord interior panel | 4 | 4-5 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord interior panel | 5 | 5-6 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord interior panel | 6 | 6-7 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord interior panel | 7 | 7-8 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord interior panel | 8 | 8-9 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord interior panel | 9 | 9-10 | L1 1/2x1 1/2x1/8[NA] | $\urcorner\ulcorner$ | 1'-8" | N/A |
| Top chord interior panel | 10 | 10-11 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord interior panel | 11 | 11-12 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-8" | N/A |
| Top chord Right second end panel (Lep |  | 12-13 | L1 1/2x1 1/2x1/8[ NA ] | าг | 2'-0" | N/A |
| Top chord right first end panel (Lep1) | 13 | 13-14 | L1 1/2x1 1/2x1/8[NA] | าг | 1'-4" | N/A |
| Bottom chord left ext. | 14 | 15-16 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | $4{ }^{\prime \prime}$ | N/A |
| Bottom chord interior panel | 15 | 16-17 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 16 | 17-18 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 17 | 18-19 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 18 | 19-20 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 19 | 20-21 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 20 | 21-22 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 21 | 22-23 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 22 | 23-24 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 23 | 24-25 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord interior panel | 24 | 25-26 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | 1'-8" | N/A |
| Bottom chord right ext. | 25 | 26-27 | L1 1/4x1 1/4x1/8[NA] | $\lrcorner\llcorner$ | $4{ }^{\prime \prime}$ | N/A |
| Left end web member | 26 | 1-16 | R7/8[NA] | $\bigcirc$ | 2'-10 9/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Aux. left or SV web member | 27 | 2-16 | R1/2[NA] | $\bigcirc$ | 1'-10 3/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior First web member | 28 | 16-3 | R3/4[NA] | 0 | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 29 | 3-17 | R3/4[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 30 | 17-4 | R5/8[NA] | 0 | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 31 | 4-18 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 32 | 18-5 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 33 | 5-19 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 34 | 19-6 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 35 | 6-20 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 36 | 20-7 | R1/2[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 37 | 7-21 | R1/2[NA] | 0 | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 38 | 21-8 | R1/2[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 39 | 8-22 | R1/2[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 40 | 22-9 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |


| B.E = Both end | Mem |  |  |  |  | Weld Information |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mem | 1-J | Designation[Reinf.] |  | Lenght | Weld Information |
| Interior web member | 41 | 9-23 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 42 | 23-10 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 43 | 10-24 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |
| Interior web member | 44 | 24-11 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Interior web member | 45 | 11-25 | R5/8[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " $; 2$ inches Both end (total lenght) |
| Interior web member | 46 | 25-12 | R3/4[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " $; 2$ inches Both end (total lenght) |
| Interior First web member | 47 | 12-26 | R3/4[NA] | $\bigcirc$ | $1^{\prime}-7$ 15/16" | Use: $1 / 8$ " $; 2$ inches Both end (total lenght) |
| Aux. right or SV web member | 48 | 26-13 | R1/2[NA] | $\bigcirc$ | $1^{\prime}-103 / 16^{\prime \prime}$ | Use: $1 / 8$ " ; 2 inches Both end (total lenght) |
| Right end web member | 49 | 26-14 | R7/8[NA] | $\bigcirc$ | 2'-10 9/16" | Use: $1 / 8{ }^{\prime \prime} ; 2$ inches Both end (total lenght) |

## GENERAL JOIST INFORMATION

## INPUT FORM ( ASD ) Revision SJI 100-2020

## Rev. 1 - Approved April 27, 2020

## General Data

**** Parallel Chord and rod web members ****
Designation $=18 \mathrm{~K} 3 \mathrm{SP}$
Depth = 18 inches; de = Effective Depth 17.220 inches
Clear Depth $=15.250$ inches
Span = $22^{\prime}-0^{\prime \prime}$
Span design $=22.000-0.333=21.667 \mathrm{ft} .=21^{\prime}-8{ }^{\prime \prime}=\mathrm{L}=260.00 \mathrm{in}$
Total Joist Weight $=137.749$ Lbs./joist
Joist Weight $=6.261309 \mathrm{Lbs} . / \mathrm{ft}$. (SJl $6.400 \mathrm{Lbs} / \mathrm{ft}$.)
Assumed Chord Spacing ( $s$ ) = 1/2"
EXTC Left Lenght end $=0$ "; EXBC Left =6"
EXTC Right Lenght end $=0$ "; EXBC Right $=6^{\prime \prime}$
Camber = 1/4"
Seat Type=Outside Seat
Left Seat Angle $=$ L2x2x5/16 x 6"; Hight = $21 / 2^{\prime \prime}$
Right Seat Angle $=\mathrm{L} 2 \times 2 \times 5 / 16 \times 6$ "; Hight $=21 / 2^{\prime \prime}$
Check Span Depth Ratio (SJI Spec 5.2)
SJI - Spec 5.2
Span*12/d = 22.00*12.0/18=14.667 ft.
Ratio $=14.67 / 24=0.61$
(Check Ratio) 0.61 <= 1.0 <<--- OK

## Seat Extender

Left seat not extender to end panel
Right seat not extender to end panel

## LOAD (SJI) (I=Interpolation)

Uniform Total SJI (TL) = (I=382.000 \#/ft) 382.000 \#/ft full lenght
Uniform Live (LL) $=(\mathrm{I}=316.000$ \#/ft) 316.000 \#/ft full lenght
Uniform Dead (DL) $=(\mathrm{l}=66.000$ \#/ft) 66.000 \#/ft full lenght

## Not Additional load present

UPLIFT ACTIVE - PATTERM \#2 (THREE LOAD)
250.000 Lbs/ft From 0 to 6'-0"
175.000 Lbs/ft From 6'-0" to 15'-8" (9'-8")
250.000 Lbs/ft From 15'-8" to 21'-8" (6'-0")

## Combination [SW=Self Weight]

COMB1 = 1.00xDL+1.00xLL + [SW F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 x D L+1.00 x U P+[S W$ F=0.60]

## (R)Reaction

Reation (Comb. \#1): Left = 4.207 Kips; Right $=4.207$ Kips
Reation (Comb. \#2): Left $=0.000$ Kips; Right $=0.000$ Kips
Reation (Comb. \#3): Left = 3.492 Kips; Right $=3.492$ Kips
Reation (Comb. \#4): Left $=-1.894$ Kips; Right $=-1.894$ Kips
Maximun Actual Deflection (Check in Red)
$1.00 x D L+1.00 x L L=-0.772$ in. (Member \#7)
$1.00 \times D L+1.00 \times L L=0.000$ in.(Member \#25)
$1.00 x L L=-0.641$ in.(Member \#7)
$0.60 x D L+1.00 x U P=0.317$ in.(Member \#7)

## Maximun Allowed Deflection (Live Load)

## Floors

Floors $=1 / 360$ of span
$=($ Span 12.0$) / 360$
$=(22.000 * 12.0) / 360=0.733 \mathrm{in}$.
Roof where plaster ceiling is attached or suspended(Rc)
$R c=1 / 360$ of span
$=($ Span 12.0$) / 360$
$=(22.000 * 12.0) / 360=0.733 \mathrm{in}$.
Roof for all other cases(Ro)
$R o=1 / 240$ of span
$=\left(\right.$ Span $\left.{ }^{*} 12.0\right) / 240$
$=\left(22.000^{*} 12.0\right) / 240=1.100 \mathrm{in}$.
Deflection Verify
Floor: $|0.000|<0.733$ OK
Roof: $\mid 0.000$ < 1.100 OK
L / 1 Live Defl.(This joist)

## Maximun Axial Force

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=-6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=-15.790$ Kips in Member \#20; Comb1
Calculate an equivalent uniform load (W) based on the maximum moment( m ) or shear( v ).
$\mathrm{Wm}=\left(8^{*} \mathrm{Jm}\right) / \mathrm{L}$ ^2
$=8^{*}(22.658) /\left(\left(21.667^{\wedge} 2\right)\right)=386.129 \mathrm{plf}$
$W v=\left(2^{*} R\right) / L$
$=2^{*}(4.207) /(21.667)=388.357$ plf
Use: $\mathrm{W}=388.357$ \#/ft. $=0.388 \mathrm{kft}$.(Joist Weight Included)

$$
\mathrm{W}=382.000 \text { \#/ft. = } 0.382 \mathrm{k} / \mathrm{ft} \text {.(Not Joist Weight Included) }
$$

## Calculate Moment

Joist moment (Jm) = max Axia force * effective depth=

$$
=15.790 * 17.220=271.900 \mathrm{k}-\mathrm{in}=22.658 \mathrm{k}-\mathrm{ft}
$$

Joist moment(SJI Manual) $=\left(w^{*}\right.$ L^2 $\left.^{\wedge}\right) / 8=$

$$
=\left(0.388^{*}\left(22.000^{\wedge} 2\right)\right) / 8.0=281.935 \mathrm{k}-\mathrm{in}=23.495 \mathrm{k}-\mathrm{ft}
$$

## Calculate Inertia Moment (Joist)

Required Moment of Inertia $=\left(1.15^{*} 5^{*} 360^{*} W L L^{*}\left(L^{*} 12\right)^{\wedge} 3\right) /\left(384^{*} \mathrm{E}\right)$ in^4

$$
=\left(1.15^{*} 5^{*} 360^{*}(0.316 / 12)^{*}\left(21.67^{*} 12\right)^{\wedge} 3\right) /\left(384^{*} 29000\right)=86.03 \text { in^4 }
$$

Moment Inertia of Joist $=86.0334$ in^4
Use Top \& Bottom chord to calculate inertia moment
Top Chord = L1 $1 / 2 \times 11 / 2 \times 1 / 8 ; \mathrm{A} 1=0.718 ; \mathrm{y} 1=0.421 ; \mathrm{Ix} 1=0.156$
Bottom Chord = L1 1/4×1 1/4×1/8; A2=0.594; y2=0.359; $1 \times 2=0.088$
Total Area(TA) $=\mathrm{A} 1+\mathrm{A} 2=0.718+0.594=1.312$
Center Gravity $(\mathrm{Cg})=\left(\left(y 1^{*} \mathrm{~A} 1\right)+\left(\mathrm{y} 2^{*} \mathrm{~A} 1\right)\right) /$ At
$=\left(\left(0.359^{*} 0.718\right)+(17.579 * 0.594)\right) / 1.312=8.155$ in from bottom
$\mathrm{Y} 1=9.424 ; \mathrm{Y} 2=7.796($ from bottom $)$
ljoist $=1 x t+1 x b+\left[\left(A t^{*} A b^{*} \mathrm{de}^{\wedge} 2 /(T A)\right]\right.$
ljoist $=0.16+0.09+\left[\left(0.72^{*} 0.59^{*} 17.22^{\wedge} 2\right) /(1.31)\right]=96.64$ in $^{\wedge} 4$
CHECK Moment Of Inertia (Required vs This Joist)
86.03 < 96.64 OK

Modulus Section Bottom (Sb) \& Modulus Section Top (St)
$\mathrm{Sx}=\mathrm{Sb}=\mathrm{Ix} / \mathrm{Y} 2 ; \mathrm{St}=\mathrm{Ix} / \mathrm{Y} 1$
$\mathrm{Sx}=\mathrm{Sb}=96.637 / 7.796=12.395 \mathrm{in}^{\wedge} 3$
St $=96.637 / 9.424=10.255$ in^3
Calculation of Radius of Gyration ( $r$ )
$\mathrm{r}=$ Sqr(Ix/Total Area)
$r=\operatorname{Sqr}(96.637 / 1.312)=8.582$ in

## AREA OF SURFACE

Area $=43.346$ sq.ft. one Joist
PRIMER
Primer = Std. Red Oxide Primer; Gal. req'd $=43.346 / 200.000=0.216732$ gals.
Gal. req'd = 1 gal.

## BRIDGING NOTES

Use normal bridging
Max. spaces of Bridging in top: 8.167 Ft. = 8'-2"
Max. spaces of Bridging in Bottom: 5.667 Ft. $=5^{\prime}-8{ }^{\prime \prime}$

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 1
Serial $=\mathrm{K}$
Member name = Top chord left first end panel (Lep1)
Type = 2Angles(\#2)(1)
Section = ᄀ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-4 "=1.333 \mathrm{ft}$. $=16.00 \mathrm{in}$.
End Panel Lenghtg (Lip) = 16 in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 120

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 6.879 | 0.129 | 0.528 | 1.141 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.528 | 0.000 |
| COMB3 | 0.000 | 5.710 | 0.107 | 0.528 | 1.141 |
| COMB4 | 3.070 | 0.000 | 0.075 | 0.528 | 1.141 |

Max. Local Shear $(\mathrm{V})=0.128767$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.095092$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044000$ K-ft; Location in COMB1
Max. Tension = 3.070 Kips; Location in COMB4
Max. Compresion $=6.879$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=1.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.333^{*} 12\right) / 0.466=34.326$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.000^{*} 12\right) / 0.817=44.063$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.333^{*} 12\right) / 0.296=54.054$

SLRtc $=$ Control $=54.054$
Comp. Ratio $=$ Control $/ 120=54.1 / 120=0.450$
Comp. Status: $0.45<1.00 \ll--$ OK
Tens. Ratio $=$ Control $/ 240=54.05 / 240=0.23$
Tens. Status: $0.23<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(1.00^{*} 1.33^{*} 12\right) / 0.30=54.05$

SLRgov=54.05
Fy=50.00 ksi;
Area=0.72 in^2;Comp=6.88 kips; fa=Comp/Area=9.58 ksi
Fcr=39.14 ksi; Fa=0.6Fcr= 23.49 ksi
IRc=fa/Fa=9.581/23.485=0.410
Comp. Status: 0.41 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(3.070 \times 1.000) / 0.718=4.276 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=4.28 / 30.00=0.14$
Status: 0.14 < 1.00 <<-- OK

## CHECK COMBINED AXIAL AND BENDING STRESSES

## End Panel

Mpp=1.141 in-K; Mpnl=0.528 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4
fbu_pp=7.893;Cm_ep=0.988; fa=fau=fc=9.58; Atc=0.72 in^2
$\mathrm{Cm}=1-0.5^{*} \mathrm{fa} / \mathrm{F}^{\prime} \mathrm{e}$
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
Kx=1.00
Fex=242.90 ksi; Fe_tc=97.96 ksi
fa/(Fa_rc) $=0.408$; Cm=1-0.5(fau/Fex) $=0.989$
IRtc_pnl=0.467
Status: $0.467<0.9 \ll--$ OK
AT THE PANEL POINT (SJI Eq. 4.4)
IRtc_pp=0.582
Status: 0.582 < 0.9 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW=45.000,Force(P)=5.847, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{tt}=\mathrm{P} / \mathrm{A}=8.144$
Evaluation Node \#1; Shear(V) $=3.949 ; f v=V /\left(b t^{*} 2^{*} t\right)=10.530 ; f v m o d=11.289$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=11.289 <= fn/OmegaW OK
Evaluation Node \#2; Shear(V) $=0.617 ; \mathfrak{f v =}=\mathrm{V} /(\mathrm{bt} * 2)=1.646 ;$ fvmod=4.392
fvmod $=(1 / 2)^{\star}\left(f t^{\wedge} 2+4 f v^{\wedge} 2\right)^{\wedge 1} / 2=4.392<=f n / O m e g a W$ OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 2
Serial $=\mathrm{K}$
Member name = Top chord left second end panel (Lep2)
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=2^{\prime}-0$ " $=2.000 \mathrm{ft}$ = 24.00 in .
End Panel Lenghtg (Lip) $=24$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 120

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Kips | Kips | Kips | K-in | K-in |  |
| COMB1 | 0.000 | 6.399 | 0.244 | 1.242 | 1.681 |
| COMB2 | 0.000 | 0.000 | 0.000 | 1.242 | 0.000 |
| COMB3 | 0.000 | 5.312 | 0.202 | 0.000 | 0.000 |
| COMB4 | 2.802 | 0.000 | 0.128 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.243579$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.140047$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.103532$ K-ft; Location in COMB1
Max. Tension = 2.802 Kips; Location in COMB4
Max. Compresion $=6.399$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=1.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(2.000^{*} 12\right) / 0.466=51.489$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.000^{*} 12\right) / 0.817=44.063$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(2.000^{*} 12\right) / 0.296=81.081$

SLRtc $=$ Control $=81.081$
Comp. Ratio $=$ Control $/ 120=81.1 / 120=0.676$
Comp. Status: 0.68 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=81.08 / 240=0.34$
Tens. Status: $0.34<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(1.00^{*} 2.00^{*} 12\right) / 0.30=81.08$

SLRgov=81.08
Fy=50.00 ksi;
Area=0.72 in^2;Comp=6.40 kips; fa=Comp/Area=8.91 ksi
Fcr=30.28 ksi; Fa=0.6Fcr= 18.17 ksi
IRc=fa/Fa=8.912/18.168=0.490
Comp. Status: 0.49 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(2.802 \times 1.000) / 0.718=3.903 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=3.90 / 30.00=0.13$
Status: 0.13 < 1.00 <<-- OK

## CHECK COMBINED AXIAL AND BENDING STRESSES

## End Panel

Mpp=1.681 in-K; Mpnl=1.242 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4
fbu_pp=11.624;Cm_ep=0.974; fa=fau=fc=8.91; Atc=0.72 in^2
$\mathrm{Cm}=1-0.5 * \mathrm{fa} / \mathrm{F}$ 'e
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
Kx=1.00
Fex=107.96 ksi; Fe_tc=43.54 ksi
$\mathrm{fa} /($ Fa_rc) $=0.491 ; \mathrm{Cm}=1-0.5$ (fau/Fex) $=0.977$
|Rtc_pnl=0.580
Status: $0.580<0.9 \ll--$ OK
AT THE PANEL POINT (SJI Eq. 4.4)
IRtc_pp=0.685
Status: 0.685 < 0.9 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force $(\mathrm{P})=5.439$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=7.575$
Evaluation Node \#2; Shear $(\mathrm{V})=0.617 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=1.646 ; \mathrm{fvmod}=4.130$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=4.130 <= fn/OmegaW OK
Evaluation Node \#3; Shear(V) = 3.343; fv=V/(bt*2)=8.914; fvmod=9.685
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.685 <=fn/OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 3
Serial $=\mathrm{K}$
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Kips | Kips | Kips | K-in | K-in |  |
| COMB1 | 0.000 | 9.813 | 0.207 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 8.146 | 0.172 | 0.531 | 1.061 |
| COMB4 | 4.219 | 0.000 | 0.109 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.207352$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 4.219 Kips; Location in COMB4
Max. Compresion = 9.813 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*}{ }^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=9.81 kips; fa=Comp/Area=13.67 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=13.668/24.077=0.570
Comp. Status: 0.57 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(4.219 \times 1.000) / 0.718=5.875 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=5.88 / 30.00=0.20$
Status: $0.20<1.00$ <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4
fbu_pp $=7.34 \mathrm{ksi} . ;$ fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=13.67; Atc=0.72 in^2
$\mathrm{Cm}=1-0.67^{*} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.568 ; \mathrm{Cm}=1-0.67(\mathrm{fau} / \mathrm{Fex})=0.967$
|Rtc_pnl=0.59
Status: $0.59<1.0 \ll--$ OK
AT THE PANEL POINT
IRtc_pnl=0.700
Status: $0.70<1.0 \ll--$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50 \mathrm{in}$, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000$;fn $\times$ OmegaW $=45.000$,Force $(P)=8.341$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=11.617$
Evaluation Node \#3; Shear $(\mathrm{V})=3.343 ; f v=\mathrm{V} /\left(\mathrm{bt}^{\star} 2^{\star t} \mathrm{t}\right)=8.914 ;$ fvmod=10.640
fvmod=(1/2)*(ft^2+4fv^2)^1/2=10.640 <= fn/OmegaW OK
Evaluation Node \#4; Shear(V) $=2.536 ; \mathfrak{f v}=\mathrm{V} /(\mathrm{bt} * 2)=6.764 ;$ fvmod=8.916 fvmod=(1/2)*(ft^2+4fv^2)^1/2=8.916 <= fn/OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 4
Serial $=\mathrm{K}$
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 12.417 | 0.166 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 10.307 | 0.137 | 0.531 | 1.061 |
| COMB4 | 5.205 | 0.000 | 0.088 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.165717$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 5.205 Kips; Location in COMB4
Max. Compresion = 12.417 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*}{ }^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=12.42 kips; fa=Comp/Area=17.29 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=17.293/24.077=0.720
Comp. Status: 0.72 <= $1.00 \ll-$ OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(5.205 \times 1.000) / 0.718=7.249 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=7.25 / 30.00=0.24$
Status: 0.24 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4 fbu_pp $=7.34 \mathrm{ksi} . ;$ fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=17.29; Atc=0.72 in^2 $\mathrm{Cm}=1-0.67^{\star} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.718 ; \mathrm{Cm}=1-0.67(\mathrm{fau} / \mathrm{Fex})=0.958$
IRtc_pnl=0.75
Status: 0.75 < 1.0 <<-- OK
AT THE PANEL POINT
IRtc_pnl=0.821
Status: 0.82 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50 \mathrm{in}$, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn $=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force(P) $=10.554$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=14.699$
Evaluation Node \#4; Shear (V) = 2.536; fv=V/(bt*2*t)=6.764; fvmod=9.988 fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.988 <= fn/OmegaW OK
Evaluation Node \#5; Shear(V) = 1.943; fv=V/(bt*2)=5.181; fvmod=8.992 fvmod=(1/2)*(ft^2+4fv^2)^1/2=8.992 <= fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 5
Serial = K
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 14.295 | 0.163 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 11.866 | 0.135 | 0.531 | 1.061 |
| COMB4 | 5.855 | 0.000 | 0.062 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.163100$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 5.855 Kips; Location in COMB4
Max. Compresion = 14.295 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*}{ }^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=14.30 kips; fa=Comp/Area=19.91 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=19.910/24.077=0.830
Comp. Status: 0.83 <= $1.00 \ll-$ OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(5.855 \times 1.000) / 0.718=8.155 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=8.15 / 30.00=0.27$
Status: 0.27 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4 fbu_pp $=7.34$ ksi.; fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=19.91; Atc=0.72 in^2 $\mathrm{Cm}=1-0.67^{\star} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.827 ; \mathrm{Cm}=1-0.67$ (fau/Fex) $=0.952$
|Rtc_pnl=0.85
Status: 0.85 < 1.0 <<-- OK
AT THE PANEL POINT
IRtc_pnl=0.908
Status: $0.91<1.0$ <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn $=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force(P) $=12.151$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=16.923$
Evaluation Node \#5; Shear $(\mathrm{V})=1.943 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{\star} \mathrm{t}\right)=5.181 ; \mathrm{fvmod}=9.922$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.922 <= fn/OmegaW OK
Evaluation Node \#6; Shear(V) = 1.289; fv=V/(bt*2)=3.437; fvmod=9.133 fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.133 <= fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 6
Serial = K
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 15.419 | 0.163 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 12.799 | 0.135 | 0.531 | 1.061 |
| COMB4 | 6.235 | 0.000 | 0.056 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.162818$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 6.235 Kips; Location in COMB4
Max. Compresion $=15.419$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=15.42 kips; fa=Comp/Area=21.48 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=21.475/24.077=0.890
Comp. Status: 0.89 <= $1.00 \ll-$ OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(6.235 \times 1.000) / 0.718=8.683 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=8.68 / 30.00=0.29$
Status: $0.29<1.00$ <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4
fbu_pp $=7.34 \mathrm{ksi} . ;$ fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=21.48; Atc=0.72 in^2
$\mathrm{Cm}=1-0.67^{*} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.892 ; \mathrm{Cm}=1-0.67$ (fau/Fex) $=0.948$
|Rtc_pnl=0.92
Status: 0.92 < 1.0 <<-- OK
AT THE PANEL POINT
IRtc_pnl=0.960
Status: $0.96<1.0 \ll-$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force $(\mathrm{P})=13.106$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=18.254$
Evaluation Node \#6; Shear $(\mathrm{V})=1.289 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{\star} \mathrm{t}\right)=3.437$; $\mathrm{fvmod}=9.752$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.752 <= fn/OmegaW OK
Evaluation Node \#7; Shear(V) $=0.910 ; f v=V /(b t * 2)=2.425 ; ~ f v m o d=9.444$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.444 <= fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 7
Serial $=\mathrm{K}$
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Kips | Kips | Kips | K-in | K-in |  |
| COMB1 | 0.000 | 15.790 | 0.160 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 13.107 | 0.133 | 0.531 | 1.061 |
| COMB4 | 6.361 | 0.000 | 0.056 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.160187$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 6.361 Kips; Location in COMB4
Max. Compresion = 15.790 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=15.79 kips; fa=Comp/Area=21.99 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=21.991/24.077=0.910
Comp. Status: 0.91 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(6.361 \times 1.000) / 0.718=8.860 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=8.86 / 30.00=0.29$
Status: $0.29<1.00$ <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4
fbu_pp $=7.34 \mathrm{ksi} . ;$ fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=21.99; Atc=0.72 in^2
$\mathrm{Cm}=1-0.67^{*} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.913 ; \mathrm{Cm}=1-0.67(\mathrm{fau} / \mathrm{Fex})=0.947$
|Rtc_pnl=0.94
Status: 0.94 < 1.0 <<-- OK
AT THE PANEL POINT
IRtc_pnl=0.978
Status: 0.98 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force( P$)=13.421$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=18.693$
Evaluation Node \#7; Shear $(\mathrm{V})=0.910 ; f v=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=2.425 ; f v m o d=9.656$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.656 <= fn/OmegaW OK
Evaluation Node \#8; Shear $(\mathrm{V})=0.910 ; f v=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2\right)=2.425$; fvmod=9.656
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.656 <= fn/OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 8
Serial $=\mathrm{K}$
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 15.419 | 0.163 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 12.799 | 0.135 | 0.531 | 1.061 |
| COMB4 | 6.235 | 0.000 | 0.056 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.162818$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 6.235 Kips; Location in COMB4
Max. Compresion = 15.419 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=15.42 kips; fa=Comp/Area=21.48 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=21.475/24.077=0.890
Comp. Status: 0.89 <= $1.00 \ll-$ OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(6.235 \times 1.000) / 0.718=8.683 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=8.68 / 30.00=0.29$
Status: $0.29<1.00$ <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4 fbu_pp $=7.34 \mathrm{ksi} . ;$ fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=21.48; Atc=0.72 in^2 $\mathrm{Cm}=1-0.67^{\star} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.892 ; \mathrm{Cm}=1-0.67$ (fau/Fex) $=0.948$
|Rtc_pnl=0.92
Status: 0.92 < 1.0 <<-- OK
AT THE PANEL POINT
IRtc_pnl=0.960
Status: 0.96 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn=30.000;fn $\times$ OmegaW $=45.000$,Force $(P)=13.106$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=18.254$
Evaluation Node \#8; Shear(V) $=0.910 ; f v=V /\left(b t^{*} 2^{*} t\right)=2.425 ; f v m o d=9.444$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.444 <= fn/OmegaW OK
Evaluation Node \#9; Shear(V) = 1.289; fv=V/(bt*2)=3.437; fvmod=9.752
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.752 <= fn/OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 9
Serial $=\mathrm{K}$
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 14.295 | 0.163 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 11.866 | 0.135 | 0.531 | 1.061 |
| COMB4 | 5.855 | 0.000 | 0.062 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.163100$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 5.855 Kips; Location in COMB4
Max. Compresion = 14.295 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=14.30 kips; fa=Comp/Area=19.91 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=19.910/24.077=0.830
Comp. Status: 0.83 <= $1.00 \ll-$ OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(5.855 \times 1.000) / 0.718=8.155 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=8.15 / 30.00=0.27$
Status: 0.27 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4 fbu_pp $=7.34$ ksi.; fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=19.91; Atc=0.72 in^2 $\mathrm{Cm}=1-0.67^{\star} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.827 ; \mathrm{Cm}=1-0.67$ (fau/Fex) $=0.952$
|Rtc_pnl=0.85
Status: 0.85 < 1.0 <<-- OK
AT THE PANEL POINT
IRtc_pnl=0.908
Status: $0.91<1.0$ <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50 \mathrm{in}$, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force $(\mathrm{P})=12.151$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=16.923$
Evaluation Node \#9; Shear $(\mathrm{V})=1.289 ; f v=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=3.437$; fvmod=9.133
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.133 <=fn/OmegaW OK
Evaluation Node \#10; Shear(V) = 1.943; fv=V/(bt*2)=5.181; fvmod=9.922 fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.922 <= fn/OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 10
Serial $=\mathrm{K}$
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 12.417 | 0.166 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 10.307 | 0.137 | 0.531 | 1.061 |
| COMB4 | 5.205 | 0.000 | 0.088 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.165717$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 5.205 Kips; Location in COMB4
Max. Compresion = 12.417 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*}{ }^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=12.42 kips; fa=Comp/Area=17.29 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=17.293/24.077=0.720
Comp. Status: 0.72 <= $1.00 \ll-$ OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(5.205 \times 1.000) / 0.718=7.249 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=7.25 / 30.00=0.24$
Status: 0.24 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4 fbu_pp $=7.34 \mathrm{ksi} . ;$ fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=17.29; Atc=0.72 in^2 $\mathrm{Cm}=1-0.67^{\star} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.718 ; \mathrm{Cm}=1-0.67(\mathrm{fau} / \mathrm{Fex})=0.958$
IRtc_pnl=0.75
Status: 0.75 < 1.0 <<-- OK
AT THE PANEL POINT
IRtc_pnl=0.821
Status: 0.82 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50 \mathrm{in}$, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn $=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force(P) $=10.554$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=14.699$
Evaluation Node \#10; Shear(V) = 1.943; fv=V/(bt*2*t)=5.181; fvmod=8.992
fvmod=(1/2)*(ft^2+4fv^2)^1/2=8.992 <= fn/OmegaW OK
Evaluation Node \#11; Shear(V) $=2.536$; $\mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2\right)=6.764$; fvmod=9.988 fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.988 <= fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 11
Serial $=\mathrm{K}$
Member name = Top chord interior panel
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Interior Panel Lenghtg (Lip) $=20$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 90

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Kips | Kips | Kips | K-in | K-in |  |
| COMB1 | 0.000 | 9.813 | 0.207 | 0.531 | 1.061 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.531 | 0.000 |
| COMB3 | 0.000 | 8.146 | 0.172 | 0.531 | 1.061 |
| COMB4 | 4.219 | 0.000 | 0.109 | 0.531 | 1.061 |

Max. Local Shear $(\mathrm{V})=0.207352$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.088426$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044213$ K-ft; Location in COMB1
Max. Tension = 4.219 Kips; Location in COMB4
Max. Compresion = 9.813 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.75

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.67^{*} 12\right) / 0.47=42.91$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.00^{*} 12\right) / 0.82=44.06$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.67^{*} 12\right) / 0.30=67.57$

SLRtc $=$ Control $=67.568$
Comp. Ratio $=$ Control $/ 90=67.6 / 90=0.751$
Comp. Status: 0.75 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=67.57 / 240=0.28$
Tens. Status: $0.28<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.75^{*} 1.67^{*} 12\right) / 0.30=50.68$

SLRgov=50.68
Fy=50.00 ksi;
Area=0.72 in^2;Comp=9.81 kips; fa=Comp/Area=13.67 ksi
Fcr=40.13 ksi; Fa=0.6Fcr= 24.08 ksi
IRc=fa/Fa=13.668/24.077=0.570
Comp. Status: 0.57 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(4.219 \times 1.000) / 0.718=5.875 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=5.88 / 30.00=0.20$
Status: $0.20<1.00$ <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=1.061 in-K; Mpnl=0.531 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4 fbu_pp $=7.34 \mathrm{ksi} . ;$ fbu_pnl $=1.43 \mathrm{ksi}$. fa=fau=fc=13.67; Atc=0.72 in^2 $\mathrm{Cm}=1-0.67^{*} \mathrm{fau} /$ Phi*F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD SJI Eqs 4.4-9 \& 4.4-10
Fex=276.39 ksi; Fe_tc=111.45 ksi
$\mathrm{fa} /($ Fa_rc $)=0.568 ; \mathrm{Cm}=1-0.67(\mathrm{fau} / \mathrm{Fex})=0.967$
|Rtc_pnl=0.59
Status: $0.59<1.0 \ll--$ OK
AT THE PANEL POINT
IRtc_pnl=0.700
Status: $0.70<1.0 \ll--$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50 \mathrm{in}$, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force $(\mathrm{P})=8.341$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=11.617$
Evaluation Node \#11; Shear(V) $=2.536 ; f v=V /\left(b t^{*} 2^{*} t\right)=6.764 ;$ fvmod $=8.916$ fvmod=(1/2)*(ft^2+4fv^2)^1/2=8.916 <= fn/OmegaW OK
Evaluation Node \#12; Shear(V) = 3.343; fv=V/(bt*2)=8.914; fvmod=10.640 fvmod=(1/2)*(ft^2+4fv^2)^1/2=10.640 <= fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 12
Serial $=\mathrm{K}$
Member name = Top chord Right second end panel (Lep2)
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=2^{\prime}-0{ }^{\prime \prime}=2.000 \mathrm{ft}$ = 24.00 in .
End Panel Lenghtg (Lip) $=24$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 120

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $x=0.156$ in $^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Kips | Kips | Kips | K-in | K-in |  |
| COMB1 | 0.000 | 6.399 | 0.244 | 1.242 | 1.681 |
| COMB2 | 0.000 | 0.000 | 0.000 | 1.242 | 0.000 |
| COMB3 | 0.000 | 5.312 | 0.202 | 0.000 | 0.000 |
| COMB4 | 2.802 | 0.000 | 0.128 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.243579$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.140047$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.103532$ K-ft; Location in COMB1
Max. Tension = 2.802 Kips; Location in COMB4
Max. Compresion $=6.399$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=1.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(2.000^{*} 12\right) / 0.466=51.489$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.000^{*} 12\right) / 0.817=44.063$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(2.000^{*} 12\right) / 0.296=81.081$

SLRtc $=$ Control $=81.081$
Comp. Ratio $=$ Control $/ 120=81.1 / 120=0.676$
Comp. Status: 0.68 < 1.00 <<-- OK
Tens. Ratio $=$ Control $/ 240=81.08 / 240=0.34$
Tens. Status: $0.34<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(1.00^{*} 2.00^{*} 12\right) / 0.30=81.08$

SLRgov=81.08
Fy=50.00 ksi;
Area=0.72 in^2;Comp=6.40 kips; fa=Comp/Area=8.91 ksi
Fcr=30.28 ksi; Fa=0.6Fcr= 18.17 ksi
IRc=fa/Fa=8.912/18.168=0.490
Comp. Status: 0.49 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(2.802 \times 1.000) / 0.718=3.903 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=3.90 / 30.00=0.13$
Status: 0.13 < 1.00 <<-- OK

## CHECK COMBINED AXIAL AND BENDING STRESSES

## End Panel

Mpp=1.681 in-K; Mpnl=1.242 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4
fbu_pp=11.624;Cm_ep=0.974; fa=fau=fc=8.91; Atc=0.72 in^2
Cm=1-0.5*fa/F'e
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
Kx=1.00
Fex=107.96 ksi; Fe_tc=43.54 ksi
$\mathrm{fa} /($ Fa_rc) $=0.491 ; \mathrm{Cm}=1-0.5$ (fau/Fex) $=0.977$
|Rtc_pnl=0.580
Status: $0.580<0.9 \ll--$ OK
AT THE PANEL POINT (SJI Eq. 4.4)
IRtc_pp=0.685
Status: 0.685 < 0.9 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW $=45.000$,Force $(\mathrm{P})=5.439$, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=7.575$
Evaluation Node \#12; Shear(V) $=3.343 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{* t}\right)=8.914 ;$ fvmod=9.685
fvmod=(1/2)*(ft^2+4fv^2)^1/2=9.685 <= fn/OmegaW OK
Evaluation Node \#13; Shear(V) $=0.617 ; \mathrm{fv}=\mathrm{V} /(\mathrm{bt} * 2)=1.646 ; \mathfrak{f v m o d}=4.130$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=4.130<=fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 13
Serial $=\mathrm{K}$
Member name = Top chord right first end panel (Lep1)
Type = 2Angles(\#2)(1)
Section = ㄱ г
Designation = L1 1/2x1 1/2x1/8 (LLV); A = 0.718^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-4$ " $=1.333 \mathrm{ft}$. $=16.00 \mathrm{in}$.
End Panel Lenghtg (Lip) $=16$ in
Braced Top Chord (Metal Panel) Ly $=36$ in
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced 120

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.718$ in $\wedge 2 ; \mathrm{k}=0.318$ inches
Inertia $\mathrm{x}=0.156 \mathrm{in}^{\wedge} 4, \mathrm{ly}=0.479 \mathrm{in}^{\wedge} 4$
$r x=0.47 \mathrm{in} ; r y=0.82 \mathrm{in} ; \mathrm{y}=0.421 \mathrm{in}$
$\mathrm{Sx}=0.145 \mathrm{in}^{\wedge} 3$
$r z=0.296 \mathrm{in} ;$ Qs $=0.961$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Kips | Kips | Kips | K-in | K-in |  |
| COMB1 | 0.000 | 6.879 | 0.129 | 0.528 | 1.141 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.528 | 0.000 |
| COMB3 | 0.000 | 5.710 | 0.107 | 0.528 | 1.141 |
| COMB4 | 3.070 | 0.000 | 0.075 | 0.528 | 1.141 |

Max. Local Shear $(\mathrm{V})=0.128767$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.095092$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.044000$ K-ft; Location in COMB1
Max. Tension = 3.070 Kips; Location in COMB4
Max. Compresion $=6.879$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=1.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

Assume there are no fillers at the midpanel of top chorrd center panel.
S.R. $x=\left(L x^{*} 12\right) / r x=\left(1.333^{*} 12\right) / 0.466=34.326$
S.R. $y=\left(L y^{*} 12\right) / r y=\left(3.000^{*} 12\right) / 0.817=44.063$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.333^{*} 12\right) / 0.296=54.054$

SLRtc $=$ Control $=54.054$
Comp. Ratio $=$ Control $/ 120=54.1 / 120=0.450$
Comp. Status: $0.45<1.00 \ll--$ OK
Tens. Ratio $=$ Control $/ 240=54.05 / 240=0.23$
Tens. Status: $0.23<1.00 \ll-$ OK
CHECK LATERAL STABILITY DURING ERECTION
Eq 5.5-2a; Eq 5.5-2b (Lenght bridging=Lbry=8.17)
L=22.00; dj=18.00; ry=0.817
Lbridging1 $\{$ EQ104.5-1a $=112.723 ;$ Lbridging2\{EQ104.5-2 $\}=138.893$
Lbrdg_gov = $112.72 \mathrm{in} ;$ Lbrdg_spcg $=98.00$ in
Control Ratio = (Lbrdg_spacg/Lbrdg_gov)=98.00/112.72=0.87
Status: 0.87 < 1.00 <<-- OK
CHECK COMPRESSION (4.2-4)
Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(1.00^{*} 1.33^{*} 12\right) / 0.30=54.05$

SLRgov=54.05
Fy=50.00 ksi;
Area=0.72 in^2;Comp=6.88 kips; fa=Comp/Area=9.58 ksi
Fcr=39.14 ksi; Fa=0.6Fcr= 23.49 ksi
IRc=fa/Fa=9.581/23.485=0.410
Comp. Status: 0.41 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(3.070 \times 1.000) / 0.718=4.276 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=4.28 / 30.00=0.14$
Status: 0.14 < 1.00 <<-- OK

## CHECK COMBINED AXIAL AND BENDING STRESSES

## End Panel

Mpp=1.141 in-K; Mpnl=0.528 in-K; btc=1.50 in.; Ytc=0.42 in. Ixtc=0.16 in^4
fbu_pp=7.893;Cm_ep=0.988; fa=fau=fc=9.58; Atc=0.72 in^2
$\mathrm{Cm}=1-0.5^{*} \mathrm{fa} / \mathrm{F}^{\prime} \mathrm{e}$
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
Kx=1.00
Fex=242.90 ksi; Fe_tc=97.96 ksi
fa/(Fa_rc) $=0.408$; Cm=1-0.5(fau/Fex) $=0.989$
IRtc_pnl=0.467
Status: $0.467<0.9 \ll--$ OK
AT THE PANEL POINT (SJI Eq. 4.4)
IRtc_pp=0.582
Status: 0.582 < 0.9 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4)

(Panel Point=Node=Joint).
Angle $\mathrm{b}=1.50$ in, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW=45.000,Force(P)=5.847, $\mathrm{b}=1.500 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{tt}=\mathrm{P} / \mathrm{A}=8.144$
Evaluation Node \#13; Shear(V) $=0.617 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=1.646 ;$ fvmod=4.392
fvmod=(1/2)*(ft^2+4fv^2)^1/2=4.392 <= fn/OmegaW OK
Evaluation Node \#14; Shear(V) = 3.949; fv=V/(bt*2)=10.530; fvmod=11.289
fvmod $=(1 / 2)^{*}\left(\mathrm{ft}^{\wedge} 2+4 f v^{\wedge} 2\right)^{\wedge} 1 / 2=11.289<=\mathrm{fn} /$ OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 14
Serial $=\mathrm{K}$
Member name = Bottom chord left ext.
Type $=2$ Angle(1)
Section = $\lrcorner\llcorner$
Designation $=L 11 / 4 \times 1$ 1/4x1/8 (SLV); $A=0.594^{\wedge} 2 ; F y=50 \mathrm{ksi}$
Reinforcement = NA;
Span design $=260.00$ in
Lenght Member $=4^{\prime \prime}=0.333 \mathrm{ft} .=4.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)
EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1
Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced $=240$

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in^2; $k=0.318$ inches
Inertia $x=0.088$ in $^{\wedge} 4, \mid y=0.308$ in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in} \wedge 3$
$r z=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500 \mathrm{in}=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 \times D L+1.00 \times L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[\mathrm{SW}$ F=0.60]
Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :---: | :--- |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 0.000 | 0.001 | 0.001 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| COMB3 | 0.000 | 0.000 | 0.001 | 0.001 | 0.000 |
| COMB4 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000507$ Kips; Location in COMB3
Max. Moment $(\mathrm{Me})=0.000000$ K-ft; Location in COMB4
Max. Moment (Mi) $=0.000113$ K-ft; Location in COMB3
Max. Tension $=0.000$ Kips; Location in COMB4
Max. Compresion $=0.000$ Kips; Location in COMB4
Original COMPRESION = NOT (Use for internal information only)
Max. Axial Force Top \& Bottom Chord Local
Max. Compr (top chord) force = 15.790 Kips in Member \#7; Comb1 Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4 Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1
S.R. $x=\left(L^{*} 12\right) / r x=\left(0.333^{*} 12\right) / 0.385=10.392$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(0.333^{*} 12\right) / 0.246=16.260$

SLRbc = Control $=94.387$

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $\mathrm{b}=1.25 \mathrm{in}$, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn=30.000;fn x OmegaW=20.000,Force $(P)=0.000 \mathrm{kips}$ $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=0.000 \mathrm{ksi}$
Evaluation Node \#16; Shear $(V)=3.949 ; f v=V /\left(b t^{*} 2\right)=12.635 ; f v m o d=12.635$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=12.635 <= fn/OmegaW OK

## CHECK MODULAR SECTION (S) Verification

Using Max. Moment
$\mathrm{S}=(\mathrm{M}) / \mathrm{Fb}=(0.001) / 30.000=0.000 \mathrm{in}$ ^3
$S=0.000$ in^3; Sx= 0.099 in^3
Ratio $=S / S x=0.000 / 0.099=0.000$
Status: $0.00<1.00 \ll-$ OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 15
Serial $=\mathrm{K}$
Member name = Bottom chord interior panel
Type $=$ 2Angle( 1 )
Section = $\lrcorner\llcorner$
Designation = L1 1/4×1 1/4x1/8 (SLV); A = 0.594^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in $^{\wedge} 2 ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in^4, $\mathrm{ly}=0.308$ in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) <br> Kips |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Kips | Kips | K-in | K-in |  |  |
| COMB1 | 8.340 | 0.000 | 0.009 | 0.001 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| COMB3 | 6.923 | 0.000 | 0.007 | 0.001 | 0.131 |
| COMB4 | 0.000 | 3.634 | 0.004 | 0.079 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.008865$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.010934$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.006558$ K-ft; Location in COMB4
Max. Tension = 8.340 Kips; Location in COMB1
Max. Compresion = 3.634 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.90

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll--$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=3.63 kips; fa=Comp/Area=6.12 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
Fcr=33.80 ksi; Fa=0.6Fcr= 20.28 ksi
IRc=fa/Fa=6.118/20.282=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(8.340 \times 1.000) / 0.594=14.040 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=14.04 / 30.00=0.47$
Status: 0.47 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.131 in-K; Mpnl=0.079 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4 fbu_pp $=1.33 \mathrm{ksi} . ;$ fbu_pnl $=0.32 \mathrm{ksi}$. fa=fau=fc=6.12; Abc=0.59 in^2
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /\left(\mathrm{Fa} \_\right.$rc) $=0.302 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.978$
|Rbc_pnl=0.31
Status: $0.31<1.0 \ll-$ OK
AT THE PANEL POINT
IRbc_pnl=0.248
Status: 0.25 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $\mathrm{b}=1.25$ in, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn=30.000;fn $\times$ OmegaW=20.000,Force(P)=7.089 kips $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=11.934 \mathrm{ksi}$
Evaluation Node \#16; Shear $(\mathrm{V})=3.949 ; f v=\mathrm{V} /\left(\mathrm{bt}^{*} 2^{*} \mathrm{t}\right)=12.635$; fvmod=13.974
fvmod=(1/2)*(ft^2+4fv^2)^1/2=13.974 <= fn/OmegaW OK
Evaluation Node \#17; Shear(V) $=2.537 ; f v=V /(b t * 2)=8.118 ; f v m o d=10.075$
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv} \wedge 2\right)^{\wedge} 1 / 2=10.075<=\mathrm{fn} /$ OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 16
Serial $=\mathrm{K}$
Member name = Bottom chord interior panel
Type $=$ 2Angle( 1 )
Section = $\lrcorner\llcorner$
Designation = L1 1/4×1 1/4x1/8 (SLV); A = 0.594^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in $^{\wedge} 2 ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in^4, $\mathrm{ly}=0.308$ in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Kips | Kips | Kips | K-in | K-in |  |
| COMB1 | 11.286 | 0.000 | 0.004 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 9.369 | 0.000 | 0.003 | 0.000 | 0.182 |
| COMB4 | 0.000 | 4.806 | 0.001 | 0.097 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.003868$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.015131$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.008093$ K-ft; Location in COMB4
Max. Tension = 11.286 Kips; Location in COMB1
Max. Compresion $=4.806$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4) $=-1.894$ Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.90

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll--$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=4.81 kips; fa=Comp/Area=8.09 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
Fcr=33.80 ksi; Fa=0.6Fcr= 20.28 ksi
IRc=fa/Fa=8.092/20.282=0.400
Comp. Status: $0.40<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(11.286 \times 1.000) / 0.594=19.000 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=19.00 / 30.00=0.63$
Status: 0.63 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.182 in-K; Mpnl=0.097 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4
fbu_pp $=1.84 \mathrm{ksi} . ;$ fbu_pnl $=0.40 \mathrm{ksi}$. fa=fau=fc=8.09; Abc=0.59 in^2
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
fa/(Fa_rc) $=0.399 ; \mathrm{Cm}=1-0.67$ (fa/Fex) $=0.971$
|Rbc_pnl=0.41
Status: $0.41<1.0 \ll--$ OK
AT THE PANEL POINT
|Rbc_pnl=0.331
Status: 0.33 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $\mathrm{b}=1.25$ in, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn=30.000;fn $\times$ OmegaW=20.000,Force(P)=9.593 kips $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=16.150 \mathrm{ksi}$
Evaluation Node \#17; Shear $(\mathrm{V})=2.537 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=8.118 ; \mathrm{fvmod}=11.450$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=11.450 <= fn/OmegaW OK
Evaluation Node \#18; Shear(V) $=1.947 ; f v=V /(b t * 2)=6.229 ; ~ f v m o d=10.199$
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv} \wedge 2\right)^{\wedge} 1 / 2=10.199<=$ fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 17
Serial $=\mathrm{K}$
Member name = Bottom chord interior panel
Type $=$ 2Angle(1)
Section = $\lrcorner\llcorner$
Designation = L1 1/4×1 1/4x1/8 (SLV); A = 0.594^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in $^{\wedge} 2 ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in^4, $\mathrm{ly}=0.308$ in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 13.545 | 0.000 | 0.002 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 11.244 | 0.000 | 0.002 | 0.000 | 0.208 |
| COMB4 | 0.000 | 5.605 | 0.001 | 0.105 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.002444$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.017340$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.008770$ K-ft; Location in COMB4
Max. Tension = 13.545 Kips; Location in COMB1
Max. Compresion $=5.605$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4) $=-1.894$ Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.90

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control $=94.387$
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll--$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=5.61 kips; fa=Comp/Area=9.44 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
Fcr=33.80 ksi; Fa=0.6Fcr= 20.28 ksi
IRc=fa/Fa=9.436/20.282=0.470
Comp. Status: $0.47<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(13.545 \times 1.000) / 0.594=22.803 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=22.80 / 30.00=0.76$
Status: $0.76<1.00 \ll--$ OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.208 in-K; Mpnl=0.105 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4 fbu_pp $=2.11 \mathrm{ksi} . ;$ fbu_pnl $=0.43 \mathrm{ksi} . \mathrm{fa}=\mathrm{fau}=\mathrm{fc}=9.44 ; \mathrm{Abc}=0.59 \mathrm{in}{ }^{\wedge} 2$
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /\left(\mathrm{Fa} \_\right.$rc) $)=0.465 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.966$
|Rbc_pnl=0.47
Status: $0.47<1.0 \ll-$ OK
AT THE PANEL POINT
|Rbc_pnl=0.385
Status: $0.38<1.0 \ll-$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $b=1.25$ in, Angle $t=0.13$ in
OmegaW =1.500;fn=30.000;fn $x$ OmegaW $=20.000$,Force $(P)=11.513$ kips $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=19.382 \mathrm{ksi}$
Evaluation Node \#18; Shear $(\mathrm{V})=1.947 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=6.229$; $\mathrm{fvmod}=11.521$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=11.521<= fn/OmegaW OK
Evaluation Node \#19; Shear $(\mathrm{V})=1.292 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2\right)=4.134 ; \mathrm{fvmod}=10.536$
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv}^{\wedge} 2\right)^{\wedge} 1 / 2=10.536<=\mathrm{fn} /$ OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 18
Serial $=\mathrm{K}$
Member name = Bottom chord interior panel
Type $=$ 2Angle(1)
Section = $\lrcorner\llcorner$
Designation $=L 11 / 4 \times 1$ 1/4x1/8 (SLV); $A=0.594^{\wedge} 2 ; F y=50 \mathrm{ksi}$
Reinforcement = NA;
Span design $=260.00$ in
Lenght Member $=1^{\prime}-8{ }^{\prime \prime}=1.667 \mathrm{ft} .=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega($ Omega $)=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding = 2.00 Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125$ in.
Weld Size(tw) = 1/8" = 0.125 in. $=2.000$
Spc's of Bridging Lbry $=5.667 \mathrm{ft}$. (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in^2 $^{\wedge} ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in $^{\wedge} 4$, ly= 0.308 in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; \mathrm{y}=0.359 \mathrm{in}$
$S x=0.099 \mathrm{in}^{\wedge} 3$
$r z=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in = 1/2"
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W F=1.00]$
COMB4 $=0.60 x D L+1.00 x U P+[S W$ F $=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 15.044 | 0.000 | 0.001 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 12.487 | 0.000 | 0.001 | 0.000 | 0.214 |
| COMB4 | 0.000 | 6.107 | 0.001 | 0.105 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.001111$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.017859$ K-ft; Location in COMB1
Max. Moment $(\mathrm{Mi})=0.008770$ K-ft; Location in COMB4
Max. Tension = 15.044 Kips; Location in COMB1
Max. Compresion $=6.107$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force


Max. Reation (Comb. \#1) $=$ 4.207 Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.00 ; \mathrm{Ky=} 0.00$; $\mathrm{Kz}=0.90$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll-$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=6.11 kips; fa=Comp/Area=10.28 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
Fcr=33.80 ksi; Fa=0.6Fcr= 20.28 ksi
IRc=fa/Fa=10.282/20.282=0.510
Comp. Status: $0.51<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(15.044 \times 1.000) / 0.594=25.326 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=25.33 / 30.00=0.84$
Status: $0.84<1.00 \ll--$ OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.214 in-K; Mpnl=0.105 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4 fbu_pp $=2.17$ ksi.; fbu_pnl $=0.43 \mathrm{ksi}$. fa=fau=fc=10.28; Abc=0.59 in^2
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /\left(\mathrm{Fa} \_\right.$rc) $)=0.507 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.963$
IRbc_pnl=0.51
Status: $0.51<1.0 \ll-$ OK
AT THE PANEL POINT
|Rbc_pnl=0.415
Status: $0.42<1.0 \ll-$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $b=1.25$ in, Angle $t=0.13$ in
OmegaW=1.500;fn=30.000;fn $\times$ OmegaW $=20.000$,Force $(P)=12.787$ kips $b=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=21.527 \mathrm{ksi}$
Evaluation Node \#19; Shear $(\mathrm{V})=1.292 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}^{*} 2^{*} \mathrm{t}\right)=4.134$; $\mathrm{fvmod}=11.530$
fvmod=(1/2)* $\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv}^{\wedge} 2\right)^{\wedge} 1 / 2=11.530<=\mathrm{fn} /$ OmegaW OK
Evaluation Node \#20; Shear $(\mathrm{V})=0.910 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2\right)=2.911$; $\mathrm{fvmod}=11.150$
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv}^{\wedge} 2\right)^{\wedge} 1 / 2=11.150<=\mathrm{fn} /$ OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 19
Serial $=\mathrm{K}$
Member name = Bottom chord interior panel
Type $=$ 2Angle( 1 )
Section = $\lrcorner\llcorner$
Designation = L1 1/4×1 1/4x1/8 (SLV); A = 0.594^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in $^{\wedge} 2 ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in^4, $\mathrm{ly}=0.308$ in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 15.790 | 0.000 | 0.004 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 13.107 | 0.000 | 0.003 | 0.000 | 0.248 |
| COMB4 | 0.000 | 6.363 | 0.001 | 0.122 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.003536$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.020694$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.010156$ K-ft; Location in COMB4
Max. Tension $=15.790$ Kips; Location in COMB1
Max. Compresion = 6.363 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4) $=-1.894$ Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.00; Ky=0.00; Kz=0.90

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll--$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=6.36 kips; fa=Comp/Area=10.71 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
$\mathrm{Fcr}=33.80 \mathrm{ksi} ; \mathrm{Fa}=0.6 \mathrm{Fcr}=20.28 \mathrm{ksi}$
IRc=fa/Fa=10.712/20.282=0.530
Comp. Status: $0.53<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(15.790 \times 1.000) / 0.594=26.583 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=26.58 / 30.00=0.89$
Status: 0.89 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.248 in-K; Mpnl=0.122 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4
fbu_pp $=2.51$ ksi.; fbu_pnl $=0.50 \mathrm{ksi}$. fa=fau=fc=10.71; Abc=0.59 in^2
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /\left(\mathrm{Fa} \_\right.$rc) $)=0.528 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.962$
|Rbc_pnl=0.54
Status: $0.54<1.0 \ll--$ OK
AT THE PANEL POINT
IRbc_pnl=0.441
Status: 0.44 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $\mathrm{b}=1.25$ in, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn=30.000;fn $\times$ OmegaW=20.000,Force(P)=13.422 kips $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=22.595 \mathrm{ksi}$
Evaluation Node \#20; Shear(V) = 0.910; fv=V/(bt*2*t)=2.911; fvmod=11.666 fvmod=(1/2)*(ft^2+4fv^2)^1/2=11.666 <= fn/OmegaW OK
Evaluation Node \#21; Shear(V) $=0.910 ; f v=V /(b t * 2)=2.911 ;$ fvmod=11.666
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv} \wedge 2\right)^{\wedge} 1 / 2=11.666<=\mathrm{fn} /$ OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 20
Serial $=\mathrm{K}$
Member name = Bottom chord interior panel
Type $=$ 2Angle(1)
Section = $\lrcorner\llcorner$
Designation = L1 1/4×1 1/4x1/8 (SLV); A = 0.594^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in $^{\wedge} 2 ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in^4, $\mathrm{ly}=0.308$ in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F $=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 15.790 | 0.000 | 0.004 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 13.107 | 0.000 | 0.003 | 0.000 | 0.248 |
| COMB4 | 0.000 | 6.363 | 0.001 | 0.122 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.003536$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.020694$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.010156$ K-ft; Location in COMB4
Max. Tension $=15.790$ Kips; Location in COMB1
Max. Compresion = 6.363 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4) $=-1.894$ Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.00 ; \mathrm{Ky=} 0.00$; $\mathrm{Kz}=0.90$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll-$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=6.36 kips; fa=Comp/Area=10.71 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
$\mathrm{Fcr}=33.80 \mathrm{ksi} ; \mathrm{Fa}=0.6 \mathrm{Fcr}=20.28 \mathrm{ksi}$
IRc=fa/Fa=10.712/20.282=0.530
Comp. Status: $0.53<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(15.790 \times 1.000) / 0.594=26.583 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=26.58 / 30.00=0.89$
Status: 0.89 < 1.00 <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.248 in-K; Mpnl=0.122 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4
fbu_pp $=2.51$ ksi.; fbu_pnl $=0.50 \mathrm{ksi}$. fa=fau=fc=10.71; Abc=0.59 in^2
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /\left(\mathrm{Fa} \_\right.$rc) $)=0.528 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.962$
|Rbc_pnl=0.54
Status: $0.54<1.0 \ll--$ OK
AT THE PANEL POINT
IRbc_pnl=0.441
Status: 0.44 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $\mathrm{b}=1.25$ in, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ;$ fn $\times$ OmegaW $=20.000$,Force $(\mathrm{P})=13.422 \mathrm{kips}$ $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=22.595 \mathrm{ksi}$
Evaluation Node \#21; Shear $(\mathrm{V})=0.910 ; f v=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=2.911$; $\mathrm{fvmod}=11.666$ fvmod=(1/2)*(ft^2+4fv^2)^1/2=11.666 <= fn/OmegaW OK
Evaluation Node \#22; Shear(V) $=0.910 ; f v=V /(b t * 2)=2.911 ;$ fvmod $=11.666$
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv} \wedge 2\right)^{\wedge} 1 / 2=11.666<=$ fn/OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 21
Serial $=\mathrm{K}$
Member name = Bottom chord interior panel
Type $=$ 2Angle(1)
Section = $\lrcorner\llcorner$
Designation = L1 1/4×1 1/4x1/8 (SLV); A = 0.594^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-8$ " $=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in $^{\wedge} 2 ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in^4, $\mathrm{ly}=0.308$ in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in}^{\wedge} 3$
$\mathrm{rz}=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F $=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[S W$ F=0.60]

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 15.044 | 0.000 | 0.001 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 12.487 | 0.000 | 0.001 | 0.000 | 0.214 |
| COMB4 | 0.000 | 6.107 | 0.001 | 0.105 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.001111$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.017859$ K-ft; Location in COMB1
Max. Moment (Mi) $=0.008770$ K-ft; Location in COMB4
Max. Tension = 15.044 Kips; Location in COMB1
Max. Compresion = 6.107 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4) $=-1.894$ Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.00 ; \mathrm{Ky=} 0.00$; $\mathrm{Kz}=0.90$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll-$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=6.11 kips; fa=Comp/Area=10.28 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
$\mathrm{Fcr}=33.80 \mathrm{ksi} ; \mathrm{Fa}=0.6 \mathrm{Fcr}=20.28 \mathrm{ksi}$
IRc=fa/Fa=10.282/20.282=0.510
Comp. Status: $0.51<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(15.044 \times 1.000) / 0.594=25.326 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=25.33 / 30.00=0.84$
Status: $0.84<1.00$ <<-- OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.214 in-K; Mpnl=0.105 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4 fbu_pp $=2.17 \mathrm{ksi} . ;$ fbu_pnl $=0.43 \mathrm{ksi}$. fa=fau=fc=10.28; Abc=0.59 in^2
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /\left(\mathrm{Fa} \_\right.$rc) $=0.507 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.963$
|Rbc_pnl=0.51
Status: $0.51<1.0 \ll-$ OK
AT THE PANEL POINT
IRbc_pnl=0.415
Status: 0.42 < 1.0 <<-- OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $\mathrm{b}=1.25$ in, Angle $\mathrm{t}=0.13$ in
OmegaW=1.500;fn=30.000;fn $\times$ OmegaW=20.000,Force $(\mathrm{P})=12.787 \mathrm{kips}$ $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=21.527 \mathrm{ksi}$
Evaluation Node \#22; Shear (V) $=0.910 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=2.911 ; \mathrm{fvmod}=11.150$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=11.150 <= fn/OmegaW OK
Evaluation Node \#23; Shear(V) = 1.292; fv=V/(bt*2)=4.134; fvmod=11.530
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv} \wedge 2\right)^{\wedge} 1 / 2=11.530<=$ fn/OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 22
Serial =K
Member name $=$ Bottom chord interior panel
Type = 2Angle(1)
Section = $\lrcorner\llcorner$
Designation $=L 11 / 4 \times 1$ 1/4x1/8 (SLV); $A=0.594^{\wedge} 2 ; F y=50 \mathrm{ksi}$
Reinforcement = NA;
Span design $=260.00$ in
Lenght Member $=1^{\prime}-8^{\prime \prime}=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega($ Omega $)=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding = 2.00 Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125$ in.
Weld Size(tw) = 1/8" = 0.125 in. $=2.000$
Spc's of Bridging Lbry $=5.667 \mathrm{ft}$. (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in^2 $^{\wedge} ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in $^{\wedge} 4$, ly= 0.308 in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; \mathrm{y}=0.359 \mathrm{in}$
$S x=0.099 \mathrm{in}^{\wedge} 3$
$r z=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in = 1/2"
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W F=1.00]$
COMB4 $=0.60 x D L+1.00 x U P+[S W$ F $=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 13.545 | 0.000 | 0.002 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 11.244 | 0.000 | 0.002 | 0.000 | 0.208 |
| COMB4 | 0.000 | 5.605 | 0.001 | 0.105 | 0.000 |

Max. Local Shear $(V)=0.002444$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.017340$ K-ft; Location in COMB1
Max. Moment $(\mathrm{Mi})=0.008770$ K-ft; Location in COMB4
Max. Tension = 13.545 Kips; Location in COMB1
Max. Compresion $=5.605$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force


Max. Reation (Comb. \#1) $=$ 4.207 Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.00 ; \mathrm{Ky=} 0.00$; $\mathrm{Kz}=0.90$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll--$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=5.61 kips; fa=Comp/Area=9.44 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
Fcr=33.80 ksi; Fa=0.6Fcr= 20.28 ksi
IRc=fa/Fa=9.436/20.282=0.470
Comp. Status: $0.47<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(13.545 \times 1.000) / 0.594=22.803 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=22.80 / 30.00=0.76$
Status: $0.76<1.00 \ll--$ OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.208 in-K; Mpnl=0.105 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4 fbu_pp $=2.11 \mathrm{ksi} . ;$ fbu_pnl $=0.43 \mathrm{ksi} . \mathrm{fa}=\mathrm{fau}=\mathrm{fc}=9.44 ; \mathrm{Abc}=0.59 \mathrm{in}{ }^{\wedge} 2$
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /(\mathrm{Fa}$ rc) $)=0.465 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.966$
IRbc_pnl=0.47
Status: $0.47<1.0 \ll-$ OK
AT THE PANEL POINT
|Rbc_pnl=0.385
Status: $0.38<1.0 \ll-$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $b=1.25$ in, Angle $t=0.13$ in
OmegaW =1.500;fn=30.000;fn $x$ OmegaW $=20.000$,Force $(P)=11.513$ kips $b=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=19.382 \mathrm{ksi}$
Evaluation Node \#23; Shear $(\mathrm{V})=1.292 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2^{*} \mathrm{t}\right)=4.134$; $\mathrm{fvmod}=10.536$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=10.536 <= fn/OmegaW OK
Evaluation Node \#24; Shear $(\mathrm{V})=1.947 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2\right)=6.229$; $\mathrm{fvmod}=11.521$
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv}^{\wedge} 2\right)^{\wedge} 1 / 2=11.521<=\mathrm{fn} /$ OmegaW OK

## DESIGN MEMBER

## INPUT FORM ( ASD ) Revision SJI 100-2020

Member Number = 23
Serial =K
Member name = Bottom chord interior panel
Type = 2Angle(1)
Section = $\lrcorner\llcorner$
Designation $=L 11 / 4 \times 1$ 1/4x1/8 (SLV); $A=0.594^{\wedge} 2 ; F y=50 \mathrm{ksi}$
Reinforcement = NA;
Span design $=260.00$ in
Lenght Member $=1^{\prime}-8^{\prime \prime}=1.667 \mathrm{ft}$. $=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega($ Omega $)=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding = 2.00 Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125$ in.
Weld Size(tw) = 1/8" = $0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry $=5.667 \mathrm{ft}$. (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in^2 $^{\wedge} ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in $^{\wedge} 4$, ly= 0.308 in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; \mathrm{y}=0.359 \mathrm{in}$
$S x=0.099 \mathrm{in}^{\wedge} 3$
$r z=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in = 1/2"
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W F=1.00]$
COMB4 $=0.60 x D L+1.00 x U P+[S W$ F $=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE Kips | C. FORCE Kips | SHEAR Kips | $\begin{aligned} & \text { MOM(Mi) } \\ & \text { K-in } \end{aligned}$ | $\begin{aligned} & \text { MOM(Me) } \\ & \text { K-in } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COMB1 | 11.286 | 0.000 | 0.004 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 9.369 | 0.000 | 0.003 | 0.000 | 0.182 |
| COMB4 | 0.000 | 4.806 | 0.001 | 0.097 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.003868$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.015131 \mathrm{~K}-\mathrm{ft}$; Location in COMB1
Max. Moment $(\mathrm{Mi})=0.008093$ K-ft; Location in COMB4
Max. Tension = 11.286 Kips; Location in COMB1
Max. Compresion $=4.806$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force


Max. Reation (Comb. \#1) $=$ 4.207 Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.00 ; \mathrm{Ky=} 0.00$; $\mathrm{Kz}=0.90$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll-$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=4.81 kips; fa=Comp/Area=8.09 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
Fcr=33.80 ksi; Fa=0.6Fcr= 20.28 ksi
IRc=fa/Fa=8.092/20.282=0.400
Comp. Status: $0.40<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(11.286 \times 1.000) / 0.594=19.000 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=19.00 / 30.00=0.63$
Status: $0.63<1.00 \ll--$ OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.182 in-K; Mpnl=0.097 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4
fbu_pp $=1.84 \mathrm{ksi} . ;$ fbu_pnl $=0.40 \mathrm{ksi} . \mathrm{fa}=\mathrm{fau}=\mathrm{fc}=8.09 ; \mathrm{Abc}=0.59 \mathrm{in}{ }^{\wedge} 2$
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /($ Fa_rc $)=0.399 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.971$
IRbc_pnl=0.41
Status: $0.41<1.0 \ll-$ OK
AT THE PANEL POINT
|Rbc_pnl=0.331
Status: $0.33<1.0 \ll-$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $b=1.25$ in, Angle $t=0.13$ in
OmegaW=1.500;fn=30.000;fn x OmegaW=20.000,Force $(P)=9.593 \mathrm{kips}$ $b=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=16.150 \mathrm{ksi}$
Evaluation Node \#24; Shear $(\mathrm{V})=1.947 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}^{*} 2^{*} \mathrm{t}\right)=6.229 ; \mathrm{fvmod}=10.199$ fvmod=(1/2)*(ft^2+4fv^2)^1/2=10.199 <= fn/OmegaW OK
Evaluation Node \#25; Shear $(\mathrm{V})=2.537 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2\right)=8.118$; $\mathrm{fvmod}=11.450$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=11.450<= fn/OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 24
Serial $=\mathrm{K}$
Member name $=$ Bottom chord interior panel
Type = 2Angle(1)
Section = $\lrcorner\llcorner$
Designation $=L 11 / 4 \times 1$ 1/4x1/8 (SLV); $A=0.594^{\wedge} 2 ; F y=50 \mathrm{ksi}$
Reinforcement = NA;
Span design $=260.00$ in
Lenght Member $=1^{\prime}-8{ }^{\prime \prime}=1.667 \mathrm{ft} .=20.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega($ Omega $)=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding = 2.00 Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125$ in.
Weld Size(tw) = 1/8" = 0.125 in. $=2.000$
Spc's of Bridging Lbry $=5.667 \mathrm{ft}$. (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio not excced $=200$
For Tension member Slenderness Ratio not excced 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in^2 $^{\wedge} ; \mathrm{k}=0.318$ inches
Inertia $x=0.088$ in $^{\wedge} 4$, ly= 0.308 in $^{\wedge} 4$
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; \mathrm{y}=0.359 \mathrm{in}$
$S x=0.099 \mathrm{in}^{\wedge} 3$
$r z=0.246 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in = 1/2"
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W F=1.00]$
COMB4 $=0.60 x D L+1.00 x U P+[S W$ F $=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) | KOM(Me) |
| :--- | :---: | :--- | :---: | :---: | :--- | K-in

Max. Local Shear $(V)=0.008865$ Kips; Location in COMB1
Max. Moment $(\mathrm{Me})=0.010934$ K-ft; Location in COMB1
Max. Moment $(\mathrm{Mi})=0.006558$ K-ft; Location in COMB4
Max. Tension = 8.340 Kips; Location in COMB1
Max. Compresion = 3.634 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force


Max. Reation (Comb. \#1) $=$ 4.207 Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.00 ; \mathrm{Ky=} 0.00$; $\mathrm{Kz}=0.90$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.667^{*} 12\right) / 0.385=51.962$
S.R. $y=\left(L^{*} 12\right) / r y=\left(5.667^{*} 12\right) / 0.720=94.387$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(1.667^{*} 12\right) / 0.246=81.301$

SLRbc = Control = 94.387
Comp. Ratio $=$ Control $/ 200=94.4 / 200=0.472$
Comp. Status: $0.47<1.00 \ll-$ OK
Tens. Ratio $=$ Control $/ 240=94.39 / 240=0.39$
Tens. Status: $0.39<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $z=\left(k z^{*} L^{*} 12\right) / r z=\left(0.900^{*} 1.67^{*} 12\right) / 0.246=73.171$

SLRgov=73.17
Fy=50.00 ksi;
Area=0.59 in^2;Comp=3.63 kips; fa=Comp/Area=6.12 ksi
Fe_bc=53.46 ksi; Fcr_bc=33.80 ksi
Fcr=33.80 ksi; Fa=0.6Fcr= 20.28 ksi
IRc=fa/Fa=6.118/20.282=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(8.340 \times 1.000) / 0.594=14.040 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6^{*} 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=14.04 / 30.00=0.47$
Status: $0.47<1.00 \ll--$ OK
CHECK COMBINED AXIAL AND BENDING STRESSES
AT THE CENTER PANEL
Mpp=0.131 in-K; Mpnl=0.079 in-K; bbc=1.25 in.; Ybc=0.36 in. Ixtc=0.09 in^4 fbu_pp $=1.33 \mathrm{ksi} . ;$ fbu_pnl $=0.32 \mathrm{ksi} . \mathrm{fa}=\mathrm{fau}=\mathrm{fc}=6.12 ; \mathrm{Abc}=0.59 \mathrm{in}{ }^{\wedge} 2$
Check Top Chord Center Panel for Combined Axial and Bending ASD
SJI Eqs 4.4-9 \& 4.4-10
$\mathrm{fa} /\left(\mathrm{Fa} \_\right.$rc) $)=0.302 ; \mathrm{Cm}=1-0.67(\mathrm{fa} / \mathrm{Fex})=0.978$
IRbc_pnl=0.31
Status: $0.31<1.0 \ll-$ OK
AT THE PANEL POINT
|Rbc_pnl=0.248
Status: $0.25<1.0 \ll-$ OK

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $b=1.25$ in, Angle $t=0.13$ in
OmegaW=1.500;fn=30.000;fn x OmegaW=20.000,Force $(P)=7.089 \mathrm{kips}$ $b=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=11.934 \mathrm{ksi}$
Evaluation Node \#25; Shear $(\mathrm{V})=2.537 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}^{*} 2^{*} \mathrm{t}\right)=8.118$; $\mathrm{fvmod}=10.075$
fvmod=(1/2)*(ft^2+4fv^2)^1/2=10.075 <= fn/OmegaW OK
Evaluation Node \#26; Shear $(\mathrm{V})=3.949 ; \mathrm{fv}=\mathrm{V} /\left(\mathrm{bt}{ }^{*} 2\right)=12.635 ; \mathrm{fvmod}=13.974$
fvmod $=(1 / 2)^{\star}\left(\mathrm{ft}^{\wedge} 2+4 \mathrm{fv}^{\wedge} 2\right)^{\wedge} 1 / 2=13.974<=\mathrm{fn} /$ OmegaW OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 25
Serial = K
Member name $=$ Bottom chord right ext.
Type $=2$ Angle(1)
Section = $\lrcorner\llcorner$
Designation = L1 1/4×1 1/4x1/8 (SLV); A = 0.594^2; Fy=50 ksi
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=4^{\prime \prime}=0.333 \mathrm{ft} .=4.00 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.125 \mathrm{in} .=2.000$
Spc's of Bridging Lbry = 5.667 ft . (Bottom Bridging)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
Slenderness Ratio not excced $=240$

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.594$ in^2; $k=0.318$ inches
Inertia $x=0.088$ in^4, ly=0.308 in^4
$r x=0.38 \mathrm{in} ; r y=0.72 \mathrm{in} ; y=0.359 \mathrm{in}$
$\mathrm{Sx}=0.099 \mathrm{in} \wedge 3$
$r z=0.246 \mathrm{in} ;$ Qs $=1.000$
Spacing between chord angles $=0.500 \mathrm{in}=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 \times D L+1.00 \times L L+[S W$ F=1.00]
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[S W$ F=1.00]
COMB4 $=0.60 x D L+1.00 x \mathrm{UP}+[\mathrm{SW}$ F=0.60]
Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 0.000 | 0.001 | 0.001 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| COMB3 | 0.000 | 0.000 | 0.001 | 0.001 | 0.000 |
| COMB4 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000507$ Kips; Location in COMB3
Max. Moment $(\mathrm{Me})=0.000000$ K-ft; Location in COMB4
Max. Moment (Mi) $=0.000113$ K-ft; Location in COMB3
Max. Tension $=0.000$ Kips; Location in COMB4
Max. Compresion $=0.000$ Kips; Location in COMB4
Original COMPRESION = NOT (Use for internal information only)
Max. Axial Force Top \& Bottom Chord Local
Max. Compr (top chord) force = 15.790 Kips in Member \#7; Comb1 Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4 Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1
S.R. $x=\left(L^{*} 12\right) / r x=\left(0.333^{*} 12\right) / 0.385=10.392$
S.R. $z=\left(L z^{*} 12\right) / r z=\left(0.333^{*} 12\right) / 0.246=16.260$

SLRbc $=$ Control $=94.387$

## CHECK SHEAR CAPACITY OF CHORD (Ref. SJI Spec. 4.4) <br> (Panel Point=Node=Joint).

Angle $\mathrm{b}=1.25 \mathrm{in}$, Angle $\mathrm{t}=0.13$ in
OmegaW $=1.500 ; \mathrm{fn}=30.000 ; \mathrm{fn} \times$ OmegaW $=20.000$,Force $(\mathrm{P})=0.000 \mathrm{kips}$ $\mathrm{b}=1.250 \mathrm{in} ; \mathrm{t}=0.125 \mathrm{in} ; \mathrm{ft}=\mathrm{P} / \mathrm{A}=0.000 \mathrm{ksi}$
Evaluation Node \#26; Shear $(\mathrm{V})=3.949 ; f v=\mathrm{V} /\left(\mathrm{bt}^{*} 2^{*} \mathrm{t}\right)=12.635$; fvmod=12.635
fvmod=(1/2)*(ft^2+4fv^2)^1/2=12.635 <= fn/OmegaW OK

## CHECK MODULAR SECTION (S) Verification

Using Max. Moment
$\mathrm{S}=(\mathrm{M}) / \mathrm{Fb}=(0.001) / 30.000=0.000 \mathrm{in}$ ^3
$S=0.000$ in^3; Sx= 0.099 in^3
Ratio $=S / S x=0.000 / 0.099=0.000$
Status: $0.00<1.00 \ll-$ OK

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 26
Serial $=\mathrm{K}$
Member name = Left end web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 7 / 8 ; \mathrm{A}=0.601^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=2^{\prime}-109 / 16^{\prime \prime}=2.880 \mathrm{ft}$. $=34.56 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.215 \mathrm{in} .=3.440$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.601$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.029$ in $^{\wedge} 4, \mathrm{ly}=0.313 \mathrm{in}^{\wedge} 4$
$r x=0.22 \mathrm{in} ; r y=0.22 \mathrm{in} ; \mathrm{y}=0.438 \mathrm{in}$
$\mathrm{rz}=0.219 \mathrm{in} ;$ Qs $=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 7.932 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 6.583 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 3.540 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 7.932 Kips; Location in COMB1
Max. Compresion = 3.540 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=3.540; Tens=7.932; seno = 0.498; Max. 25\% Reaction
Vertical Shear(Tens) $=3.949$; Vertical Shear(Comp) $=1.762$
Max. Tension = 7.932 Kips; ( Not Change)
Max. Compresion = 3.540 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.80$; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(2.880^{*} 12\right) / 0.219=158.000$
S.R. $y=\left(L^{*} 12\right) / r y=\left(2.880^{*} 12\right) / 0.219=158.000$
S.R. $z=\left(L^{*} 12\right) / r z=\left(2.880^{*} 12\right) / 0.219=158.000$

Control $=158.000$
Comp. Ratio $=$ Control/200 $=158.00 / 200=0.79$
Comp. Status: $0.79<1.00 \ll--$ OK
Tens. Ratio $=$ Contro $/ 240=158.00 / 240=0.66$
Tens. Status: 0.66 < 1.00 <<-- OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 2.88^{\star} 12\right) / 0.219=118.500$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.800^{*} 2.88^{*} 12\right) / 0.219=126.400$

SLRgov=126.40
Fy=50.00 ksi;
Area=0.60 in^2;Comp=3.54 kips; fa=Comp/Area=5.89 ksi
$\mathrm{Fe}=17.91 \mathrm{ksi} ; \mathrm{Fcr}=15.71 \mathrm{ksi}$
Fcr=15.71 ksi; Fa=0.6Fcr= 9.43 ksi
IRc=fa/Fa=5.887/9.427=0.620
Comp. Status: 0.62 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens x factor/Area $=(7.932 \times 1.000) / 0.601=13.191 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 \star 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=13.19 / 30.00=0.44$
Status: $0.44<=0.90^{* * *} \ll--$ OK
${ }^{* * *}$ Refer to Section 1.2B for applicationb of and the requirement for the use of the 0.90 Stress Interaction
Ratio for design check of first end web.

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=7.932; weld size = 1/8"
Lenght weld $=$ Force $\times \mathrm{OMEGAw} /\left(2^{*}\right.$ Fnw x tef $)$
Lenght weld $=7.932 \times 2.0 /(2 \times 42.000 .215)=0.878$ in.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]

## CHECK ECCENTRICITY (4.5.4)

Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 27
Serial $=\mathrm{K}$
Member name = Aux. left or SV web member
Type $=$ Single(2)
Section = 0
Designation $=\mathrm{R} 1 / 2 ; \mathrm{A}=0.196^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-103 / 16$ " $=1.849 \mathrm{ft}$. $=22.19 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.170 \mathrm{in} .=2.720$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.196$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.003$ in^4, ly $=0.052$ in^4
$r x=0.13 \mathrm{in} ; r y=0.13 \mathrm{in} ; \mathrm{y}=0.250 \mathrm{in}$
$r z=0.125 \mathrm{in} ;$ Qs $=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 0.761 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 0.630 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.425 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.425$ Kips; Location in COMB4
Max. Compresion $=0.761$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.90$; $\mathrm{Kz}=0.00$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force = 15.790 Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4 Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## For Interior Vertical Member.

gravity load +1/2 of 1.0\% of Max. Top Chord Axial Force
Tension $=\mathrm{g}+1 / 2\left(1 \%{ }^{*}\right.$ Pep $)=$
Tension $=0.425$ Kips $+0.5(0.01 * 3.070100$ Kips $)=0.440$ Kips
Max. Tension $=0.440 \mathrm{Kips} ;($ Change $)$
Compresion $=g+1 / 2(1 \% *$ Pep $)=$
Compresion $=0.761$ Kips $+0.5\left(0.01^{*} 15.789752\right.$ Kips $)=0.796$ Kips
Max. Compresion = 0.840 Kips;(Change)

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.849^{*} 12\right) / 0.125=177.500$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.849^{*} 12\right) / 0.125=177.500$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.849^{*} 12\right) / 0.125=177.500$

Control $=177.500$
Comp. Ratio $=$ Control/200 $=177.50 / 200=0.89$
Comp. Status: $0.89<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=177.50 / 240=0.74$
Tens. Status: 0.74 < $1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.85^{*} 12\right) / 0.125=133.125$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.85^{*} 12\right) / 0.125=159.750$

SLRgov=159.75
Fy=50.00 ksi;
Area=0.20 in^2;Comp=0.84 kips; fa=Comp/Area=4.28 ksi
$\mathrm{Fe}=11.22 \mathrm{ksi}$; Fcr=9.84 ksi
Fcr $=9.84 \mathrm{ksi} ;$ Fa=0.6Fcr= $=5.90 \mathrm{ksi}$
IRc=fa/Fa=4.279/5.902=0.730
Comp. Status: 0.73 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.440 \times 1.000) / 0.196=2.242 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.24 / 30.00=0.07$
Status: $0.07<1.00 \ll-$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=0.840$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=0.840 \times 2.0 /(2 \times 42.000 .170)=0.118 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 28
Serial $=\mathrm{K}$
Member name $=$ Interior First web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 3 / 4 ; \mathrm{A}=0.442^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.200 \mathrm{in} .=3.200$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.442$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.016$ in $^{\wedge} 4, \mathrm{ly}=0.188$ in $^{\wedge} 4$
$r x=0.19 \mathrm{in} ; r y=0.19 \mathrm{in} ; \mathrm{y}=0.375 \mathrm{in}$
$\mathrm{rz}=0.188 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 3.865 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 3.208 | 0.000 | 0.000 | 0.000 |
| COMB4 | 1.657 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 1.657 Kips; Location in COMB4
Max. Compresion = 3.865 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4) $=-1.894$ Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=3.865; Tens=1.657; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.433$; Vertical Shear(Comp) $=3.343$
Max. Tension = 1.657 Kips; ( Not Change)
Max. Compresion = 3.865 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.188=106.333$

Control $=106.333$
Comp. Ratio $=$ Control/200 $=106.33 / 200=0.53$
Comp. Status: $0.53<1.00 \ll-$ OK
Tens. Ratio $=$ Control/ $240=106.33 / 240=0.44$
Tens. Status: 0.44 < $1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.188=79.750$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.188=95.700$

SLRgov=95.70
Fy=50.00 ksi;
Area=0.44 in^2;Comp=3.87 kips; fa=Comp/Area=8.75 ksi
Fe=31.25 ksi; Fcr=25.59 ksi
Fcr=25.59 ksi; Fa=0.6Fcr= 15.36 ksi
IRc=fa/Fa=8.750/15.357=0.570
Comp. Status: 0.57 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(1.657 \times 1.000) / 0.442=3.751 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=3.75 / 30.00=0.13$
Status: $0.13<1.00 \ll-$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=3.865; weld size $=1 / 8^{\prime \prime}$
Lenght weld = Force $\times$ OMEGAw/(2 * Fnw $x$ tef )
Lenght weld $=3.865 \times 2.0 /(2 \times 42.000 .200)=0.460 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 29
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 3 / 4 ; \mathrm{A}=0.442^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.200 \mathrm{in} .=3.200$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.442$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.016$ in $^{\wedge} 4, \mathrm{ly}=0.188$ in $^{\wedge} 4$
$r x=0.19 \mathrm{in} ; r y=0.19 \mathrm{in} ; \mathrm{y}=0.375 \mathrm{in}$
$\mathrm{rz}=0.188 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 2.934 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 2.436 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 1.163 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment (Mi) $=0.000000$ K-ft; Location in COMB4
Max. Tension = 2.934 Kips; Location in COMB1
Max. Compresion = 1.163 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=1.163; Tens=2.934; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=2.537$; Vertical Shear(Comp) $=1.006$
Max. Tension = 2.934 Kips; ( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.188=106.333$

Control $=106.333$
Comp. Ratio $=$ Control/200 $=106.33 / 200=0.53$
Comp. Status: $0.53<1.00 \ll-$ OK
Tens. Ratio $=$ Control/ $240=106.33 / 240=0.44$
Tens. Status: 0.44 < $1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.188=79.750$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.188=95.700$

SLRgov=95.70
Fy=50.00 ksi;
Area=0.44 in^2;Comp=1.05 kips; fa=Comp/Area=2.38 ksi
$\mathrm{Fe}=31.25 \mathrm{ksi} ; \mathrm{Fcr}=25.59 \mathrm{ksi}$
Fcr=25.59 ksi; Fa=0.6Fcr= 15.36 ksi
IRc=fa/Fa=2.381/15.357=0.160
Comp. Status: 0.16 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(2.934 \times 1.000) / 0.442=6.640 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=6.64 / 30.00=0.22$
Status: $0.22<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.934; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.934 \times 2.0 /(2 \times 42.000 .200)=0.349 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 30
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 2.933 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 2.434 | 0.000 | 0.000 | 0.000 |
| COMB4 | 1.171 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 1.171 Kips ; Location in COMB4
Max. Compresion = 2.933 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=2.933; Tens=1.171; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.012$; Vertical Shear(Comp) $=2.536$
Max. Tension = 1.171 Kips;( Not Change)
Max. Compresion = 2.933 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=2.93 kips; fa=Comp/Area=9.56 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=9.560/11.420=0.840
Comp. Status: 0.84 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(1.171 \times 1.000) / 0.307=3.815 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=3.82 / 30.00=0.13$
Status: $0.13<1.00 \ll-$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.933; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.933 \times 2.0 /(2 \times 42.000 .185)=0.377 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 31
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 2.251 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 1.869 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 0.793 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 2.251 Kips; Location in COMB1
Max. Compresion $=0.793$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.793; Tens=2.251; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.947$; Vertical Shear(Comp) $=0.686$
Max. Tension = 2.251 Kips;( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.05 kips; fa=Comp/Area=3.43 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=3.428/11.420=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(2.251 \times 1.000) / 0.307=7.337 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=7.34 / 30.00=0.25$
Status: $0.25<1.00 \ll--$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.251; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.251 \times 2.0 /(2 \times 42.000 .185)=0.290 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 32
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 2.247 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 1.864 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.797 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 0.797 Kips; Location in COMB4
Max. Compresion = 2.247 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=2.247; Tens=0.797; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.689$; Vertical Shear(Comp) $=1.943$
Max. Tension $=0.797$ Kips; ( Not Change)
Max. Compresion = 2.247 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=2.25 kips; fa=Comp/Area=7.32 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr=19.03 ksi; Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=7.323/11.420=0.640
Comp. Status: 0.64 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.797 \times 1.000) / 0.307=2.599 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.60 / 30.00=0.09$
Status: $0.09<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.247; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.247 \times 2.0 /(2 \times 42.000 .185)=0.289 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 33
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 1.494 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 1.241 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 0.498 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 1.494 Kips; Location in COMB1
Max. Compresion $=0.498$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.498; Tens=1.494; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.292$; Vertical Shear(Comp) $=0.431$
Max. Tension = $1.494 \mathrm{Kips} ;$ ( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control $/ 200=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.05 kips; fa=Comp/Area=3.43 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=3.428/11.420=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(1.494 \times 1.000) / 0.307=4.870 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=4.87 / 30.00=0.16$
Status: $0.16<1.00 \ll--$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.494$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.494 \times 2.0 /(2 \times 42.000 .185)=0.192 \mathrm{in}$.
Use: $1 / 8$ " $; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 34
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4$, ly $=0.105$ in^^ $^{\wedge}$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 1.490 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 1.236 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.502 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.502$ Kips; Location in COMB4
Max. Compresion $=1.490$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=1.490; Tens=0.502; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.434$; Vertical Shear(Comp) $=1.289$
Max. Tension $=0.548 \mathrm{Kips}$ (Change)
Max. Compresion $=1.490$ Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control = 127.600
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.49 kips; fa=Comp/Area=4.86 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=4.858/11.420=0.430
Comp. Status: 0.43 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.548 \times 1.000) / 0.307=1.785 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=1.78 / 30.00=0.06$
Status: $0.06<1.00 \ll--$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.490$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.490 \times 2.0 /(2 \times 42.000 .185)=0.192 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 35
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.748 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.621 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 0.253 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.748$ Kips; Location in COMB1
Max. Compresion $=0.253$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.253; Tens=0.748; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.647$; Vertical Shear(Comp) $=0.219$
Max. Tension $=0.748 \mathrm{Kips} ;$ ( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.05 kips; fa=Comp/Area=3.43 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=3.428/11.420=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.748 \times 1.000) / 0.307=2.437 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.44 / 30.00=0.08$
Status: $0.08<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.052$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.052 \times 2.0 /(2 \times 42.000 .185)=0.135 \mathrm{in}$.
Use: $1 / 8$ " $; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 36
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 1 / 2 ; \mathrm{A}=0.196^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.170 \mathrm{in} .=2.720$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.196$ in^2 $^{\wedge} \mathrm{k}=0.318$ inches
Inertia $x=0.003$ in $^{\wedge} 4, \mathrm{ly}=0.052 \mathrm{in}^{\wedge} 4$
$r x=0.13 \mathrm{in} ; r y=0.13 \mathrm{in} ; \mathrm{y}=0.250 \mathrm{in}$
$\mathrm{rz}=0.125 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 0.739 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 0.613 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.255 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment (Mi) $=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.255$ Kips; Location in COMB4
Max. Compresion $=0.739$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.739; Tens=0.255; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.221$; Vertical Shear(Comp) $=0.639$
Max. Tension $=0.548 \mathrm{Kips}$ (Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.90$; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.125=159.500$

Control $=159.500$
Comp. Ratio $=$ Control/200 $=159.50 / 200=0.80$
Comp. Status: $0.80<1.00 \ll-$ OK
Tens. Ratio $=$ Control/240 $=159.50 / 240=0.66$
Tens. Status: 0.66 < 1.00 <<-- OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{\star} 12\right) / 0.125=119.625$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.125=143.550$

SLRgov=143.55
Fy=50.00 ksi;
Area=0.20 in^2;Comp=1.05 kips; fa=Comp/Area=5.36 ksi
$\mathrm{Fe}=13.89 \mathrm{ksi} ; \mathrm{Fcr}=12.18 \mathrm{ksi}$
Fcr=12.18 ksi; Fa=0.6Fcr= 7.31 ksi
IRc=fa/Fa=5.357/7.309=0.730
Comp. Status: 0.73 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.548 \times 1.000) / 0.196=2.789 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.79 / 30.00=0.09$
Status: $0.09<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.052$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.052 \times 2.0 /(2 \times 42.000 .170)=0.147 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 37
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 1 / 2 ; \mathrm{A}=0.196^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.170 \mathrm{in} .=2.720$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.196$ in^2 $^{\wedge} \mathrm{k}=0.318$ inches
Inertia $x=0.003$ in $^{\wedge} 4, \mathrm{ly}=0.052 \mathrm{in}^{\wedge} 4$
$r x=0.13 \mathrm{in} ; r y=0.13 \mathrm{in} ; \mathrm{y}=0.250 \mathrm{in}$
$\mathrm{rz}=0.125 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE | C. FORCE | SHEAR | MOM(Mi) | MOM(Me) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kips | Kips | Kips | K-in | K-in |
| COMB1 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.003 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment (Mi) $=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.003$ Kips; Location in COMB4
Max. Compresion $=0.001$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.001; Tens=0.003; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.002$; Vertical Shear(Comp) $=0.000$
Max. Tension $=0.548 \mathrm{Kips}$ (Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.90$; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.125=159.500$

Control $=159.500$
Comp. Ratio $=$ Control/200 $=159.50 / 200=0.80$
Comp. Status: $0.80<1.00 \ll-$ OK
Tens. Ratio $=$ Control/240 $=159.50 / 240=0.66$
Tens. Status: 0.66 < 1.00 <<-- OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{\star} 12\right) / 0.125=119.625$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.125=143.550$

SLRgov=143.55
Fy=50.00 ksi;
Area=0.20 in^2;Comp=1.05 kips; fa=Comp/Area=5.36 ksi
$\mathrm{Fe}=13.89 \mathrm{ksi} ; \mathrm{Fcr}=12.18 \mathrm{ksi}$
Fcr=12.18 ksi; Fa=0.6Fcr= 7.31 ksi
IRc=fa/Fa=5.357/7.309=0.730
Comp. Status: 0.73 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.548 \times 1.000) / 0.196=2.789 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.79 / 30.00=0.09$
Status: $0.09<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.052$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.052 \times 2.0 /(2 \times 42.000 .170)=0.147 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 38
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 1 / 2 ; \mathrm{A}=0.196^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design $=260.00$ in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.170 \mathrm{in} .=2.720$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.196$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.003$ in $^{\wedge} 4, \mathrm{ly}=0.052 \mathrm{in}^{\wedge} 4$
$r x=0.13 \mathrm{in} ; r y=0.13 \mathrm{in} ; \mathrm{y}=0.250 \mathrm{in}$
$\mathrm{rz}=0.125 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.003 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment (Mi) $=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.003$ Kips; Location in COMB4
Max. Compresion $=0.001$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.001; Tens=0.003; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.002$; Vertical Shear(Comp) $=0.000$
Max. Tension $=0.548 \mathrm{Kips}$ (Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.90$; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.125=159.500$

Control $=159.500$
Comp. Ratio $=$ Control/200 $=159.50 / 200=0.80$
Comp. Status: $0.80<1.00 \ll-$ OK
Tens. Ratio $=$ Control/240 $=159.50 / 240=0.66$
Tens. Status: 0.66 < 1.00 <<-- OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{\star} 12\right) / 0.125=119.625$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.125=143.550$

SLRgov=143.55
Fy=50.00 ksi;
Area=0.20 in^2;Comp=1.05 kips; fa=Comp/Area=5.36 ksi
$\mathrm{Fe}=13.89 \mathrm{ksi} ; \mathrm{Fcr}=12.18 \mathrm{ksi}$
Fcr=12.18 ksi; Fa=0.6Fcr= 7.31 ksi
IRc=fa/Fa=5.357/7.309=0.730
Comp. Status: 0.73 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.548 \times 1.000) / 0.196=2.789 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.79 / 30.00=0.09$
Status: $0.09<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.052$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.052 \times 2.0 /(2 \times 42.000 .170)=0.147 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 39
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 1 / 2 ; \mathrm{A}=0.196^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.170 \mathrm{in} .=2.720$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.196$ in^2 $^{\wedge} \mathrm{k}=0.318$ inches
Inertia $x=0.003$ in $^{\wedge} 4, \mathrm{ly}=0.052 \mathrm{in}^{\wedge} 4$
$r x=0.13 \mathrm{in} ; r y=0.13 \mathrm{in} ; \mathrm{y}=0.250 \mathrm{in}$
$\mathrm{rz}=0.125 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 0.739 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 0.613 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.255 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment (Mi) $=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.255$ Kips; Location in COMB4
Max. Compresion $=0.739$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.739; Tens=0.255; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.221$; Vertical Shear(Comp) $=0.639$
Max. Tension $=0.548 \mathrm{Kips}$ (Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.90$; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.125=159.500$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.125=159.500$

Control $=159.500$
Comp. Ratio $=$ Control/200 $=159.50 / 200=0.80$
Comp. Status: $0.80<1.00 \ll-$ OK
Tens. Ratio $=$ Control/240 $=159.50 / 240=0.66$
Tens. Status: 0.66 < 1.00 <<-- OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{\star} 12\right) / 0.125=119.625$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.125=143.550$

SLRgov=143.55
Fy=50.00 ksi;
Area=0.20 in^2;Comp=1.05 kips; fa=Comp/Area=5.36 ksi
$\mathrm{Fe}=13.89 \mathrm{ksi} ; \mathrm{Fcr}=12.18 \mathrm{ksi}$
Fcr=12.18 ksi; Fa=0.6Fcr= 7.31 ksi
IRc=fa/Fa=5.357/7.309=0.730
Comp. Status: 0.73 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.548 \times 1.000) / 0.196=2.789 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.79 / 30.00=0.09$
Status: $0.09<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.052$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.052 \times 2.0 /(2 \times 42.000 .170)=0.147 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 40
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.748 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.621 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 0.253 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.748$ Kips; Location in COMB1
Max. Compresion $=0.253$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.253; Tens=0.748; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.647$; Vertical Shear(Comp) $=0.219$
Max. Tension $=0.748 \mathrm{Kips} ;$ ( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.05 kips; fa=Comp/Area=3.43 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=3.428/11.420=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.748 \times 1.000) / 0.307=2.437 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.44 / 30.00=0.08$
Status: $0.08<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.052$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.052 \times 2.0 /(2 \times 42.000 .185)=0.135 \mathrm{in}$.
Use: $1 / 8$ " $; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 41
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 1.490 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 1.236 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.502 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.502$ Kips; Location in COMB4
Max. Compresion $=1.490$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=1.490; Tens=0.502; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.434$; Vertical Shear(Comp) $=1.289$
Max. Tension $=0.548 \mathrm{Kips}$ (Change)
Max. Compresion $=1.490$ Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.90$; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control = 127.600
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.49 kips; fa=Comp/Area=4.86 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=4.858/11.420=0.430
Comp. Status: 0.43 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.548 \times 1.000) / 0.307=1.785 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=1.78 / 30.00=0.06$
Status: $0.06<1.00 \ll--$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.490$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.490 \times 2.0 /(2 \times 42.000 .185)=0.192 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 42
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design $=260.00$ in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4$, ly $=0.105$ in^^ $^{\wedge}$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 1.494 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 1.241 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 0.498 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 1.494 Kips; Location in COMB1
Max. Compresion $=0.498$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.498; Tens=1.494; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.292$; Vertical Shear(Comp) $=0.431$
Max. Tension = $1.494 \mathrm{Kips} ;$ ( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control $/ 200=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.05 kips; fa=Comp/Area=3.43 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=3.428/11.420=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(1.494 \times 1.000) / 0.307=4.870 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=4.87 / 30.00=0.16$
Status: $0.16<1.00 \ll--$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=1.494$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=1.494 \times 2.0 /(2 \times 42.000 .185)=0.192 \mathrm{in}$.
Use: $1 / 8$ " $; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 43
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 2.247 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 1.864 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.797 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment (Mi) $=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.797$ Kips; Location in COMB4
Max. Compresion = 2.247 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=2.247; Tens=0.797; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=0.689$; Vertical Shear(Comp) $=1.943$
Max. Tension $=0.797$ Kips; ( Not Change)
Max. Compresion = 2.247 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=2.25 kips; fa=Comp/Area=7.32 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr=19.03 ksi; Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=7.323/11.420=0.640
Comp. Status: 0.64 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.797 \times 1.000) / 0.307=2.599 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.60 / 30.00=0.09$
Status: $0.09<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.247; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.247 \times 2.0 /(2 \times 42.000 .185)=0.289 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 44
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 2.251 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 1.869 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 0.793 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 2.251 Kips; Location in COMB1
Max. Compresion $=0.793$ Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=0.793; Tens=2.251; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.947$; Vertical Shear(Comp) $=0.686$
Max. Tension = 2.251 Kips;( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=1.05 kips; fa=Comp/Area=3.43 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=3.428/11.420=0.300
Comp. Status: $0.30<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(2.251 \times 1.000) / 0.307=7.337 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=7.34 / 30.00=0.25$
Status: $0.25<1.00 \ll--$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.251; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.251 \times 2.0 /(2 \times 42.000 .185)=0.290 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 45
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 5 / 8 ; \mathrm{A}=0.307^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio = 1.00
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.185 \mathrm{in} .=2.960$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.307$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.007$ in $^{\wedge} 4, \mathrm{ly}=0.105 \mathrm{in}^{\wedge} 4$
$r x=0.16 \mathrm{in} ; r y=0.16 \mathrm{in} ; \mathrm{y}=0.313 \mathrm{in}$
$\mathrm{rz}=0.156 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 2.933 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 2.434 | 0.000 | 0.000 | 0.000 |
| COMB4 | 1.171 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 1.171 Kips ; Location in COMB4
Max. Compresion = 2.933 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=2.933; Tens=1.171; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.012$; Vertical Shear(Comp) $=2.536$
Max. Tension = 1.171 Kips;( Not Change)
Max. Compresion = 2.933 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.156=127.600$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.156=127.600$

Control $=127.600$
Comp. Ratio $=$ Control/200 $=127.60 / 200=0.64$
Comp. Status: $0.64<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=127.60 / 240=0.53$
Tens. Status: $0.53<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.156=95.700$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.156=114.840$

SLRgov=114.84
Fy=50.00 ksi;
Area=0.31 in^2;Comp=2.93 kips; fa=Comp/Area=9.56 ksi
$\mathrm{Fe}=21.70 \mathrm{ksi} ; \mathrm{Fcr}=19.03 \mathrm{ksi}$
Fcr= $19.03 \mathrm{ksi} ;$ Fa=0.6Fcr= 11.42 ksi
IRc=fa/Fa=9.560/11.420=0.840
Comp. Status: 0.84 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(1.171 \times 1.000) / 0.307=3.815 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=3.82 / 30.00=0.13$
Status: $0.13<1.00 \ll-$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.933; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.933 \times 2.0 /(2 \times 42.000 .185)=0.377 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 46
Serial $=\mathrm{K}$
Member name = Interior web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 3 / 4 ; \mathrm{A}=0.442^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16^{\prime \prime}=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.200 \mathrm{in} .=3.200$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.442$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.016$ in $^{\wedge} 4, \mathrm{ly}=0.188$ in $^{\wedge} 4$
$r x=0.19 \mathrm{in} ; r y=0.19 \mathrm{in} ; \mathrm{y}=0.375 \mathrm{in}$
$\mathrm{rz}=0.188 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 2.934 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 2.436 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 1.163 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment (Mi) $=0.000000$ K-ft; Location in COMB4
Max. Tension = 2.934 Kips; Location in COMB1
Max. Compresion = 1.163 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=1.163; Tens=2.934; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=2.537$; Vertical Shear(Comp) $=1.006$
Max. Tension = 2.934 Kips; ( Not Change)
Max. Comp = 1.052 Kips (Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.188=106.333$

Control $=106.333$
Comp. Ratio $=$ Control/200 $=106.33 / 200=0.53$
Comp. Status: $0.53<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=106.33 / 240=0.44$
Tens. Status: 0.44 < $1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.188=79.750$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.188=95.700$

SLRgov=95.70
Fy=50.00 ksi;
Area=0.44 in^2;Comp=1.05 kips; fa=Comp/Area=2.38 ksi
$\mathrm{Fe}=31.25 \mathrm{ksi} ; \mathrm{Fcr}=25.59 \mathrm{ksi}$
Fcr=25.59 ksi; Fa=0.6Fcr= 15.36 ksi
IRc=fa/Fa=2.381/15.357=0.160
Comp. Status: 0.16 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(2.934 \times 1.000) / 0.442=6.640 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=6.64 / 30.00=0.22$
Status: $0.22<1.00$ <<-- OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=2.934; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=2.934 \times 2.0 /(2 \times 42.000 .200)=0.349 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 47
Serial $=\mathrm{K}$
Member name $=$ Interior First web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 3 / 4 ; \mathrm{A}=0.442^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-715 / 16 "=1.661 \mathrm{ft}$. $=19.94 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.200 \mathrm{in} .=3.200$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.442$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.016$ in $^{\wedge} 4, \mathrm{ly}=0.188$ in $^{\wedge} 4$
$r x=0.19 \mathrm{in} ; r y=0.19 \mathrm{in} ; \mathrm{y}=0.375 \mathrm{in}$
$r z=0.188 \mathrm{in} ;$ Qs $=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 3.865 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 3.208 | 0.000 | 0.000 | 0.000 |
| COMB4 | 1.657 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 1.657 Kips; Location in COMB4
Max. Compresion = 3.865 Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=3.865; Tens=1.657; seno = 0.865; Max. 25\% Reaction
Vertical Shear(Tens) $=1.433$; Vertical Shear(Comp) $=3.343$
Max. Tension = 1.657 Kips; ( Not Change)
Max. Compresion = 3.865 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) Kx=0.75; Ky=0.90; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.661^{*} 12\right) / 0.188=106.333$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.661^{*} 12\right) / 0.188=106.333$

Control $=106.333$
Comp. Ratio $=$ Control/200 $=106.33 / 200=0.53$
Comp. Status: $0.53<1.00 \ll-$ OK
Tens. Ratio $=$ Control/ $240=106.33 / 240=0.44$
Tens. Status: 0.44 < $1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.66^{*} 12\right) / 0.188=79.750$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.66^{*} 12\right) / 0.188=95.700$

SLRgov=95.70
Fy=50.00 ksi;
Area=0.44 in^2;Comp=3.87 kips; fa=Comp/Area=8.75 ksi
Fe=31.25 ksi; Fcr=25.59 ksi
Fcr=25.59 ksi; Fa=0.6Fcr= 15.36 ksi
IRc=fa/Fa=8.750/15.357=0.570
Comp. Status: 0.57 <= 1.00 <<-- OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(1.657 \times 1.000) / 0.442=3.751 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=3.75 / 30.00=0.13$
Status: $0.13<1.00 \ll-$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=3.865; weld size $=1 / 8^{\prime \prime}$
Lenght weld = Force $\times$ OMEGAw/(2 * Fnw $x$ tef )
Lenght weld $=3.865 \times 2.0 /(2 \times 42.000 .200)=0.460 \mathrm{in}$.
Use: $1 / 8$ " ; 2 inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 48
Serial $=\mathrm{K}$
Member name = Aux. right or SV web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 1 / 2 ; \mathrm{A}=0.196^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member = $1^{\prime}-103 / 16$ " $=1.849 \mathrm{ft}$. $=22.19 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.170 \mathrm{in} .=2.720$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.196$ in^2; $k=0.318$ inches
Inertia $x=0.003$ in^4, ly $=0.052$ in^4
$r x=0.13 \mathrm{in} ; r y=0.13 \mathrm{in} ; \mathrm{y}=0.250 \mathrm{in}$
$\mathrm{rz}=0.125 \mathrm{in} ; \mathrm{Qs}=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 \times L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 0.000 | 0.761 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 0.000 | 0.630 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.425 | 0.000 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension $=0.425$ Kips; Location in COMB4
Max. Compresion $=0.761$ Kips; Location in COMB1
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.90$; $\mathrm{Kz}=0.00$

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force = 15.790 Kips in Member \#7; Comb1 Max. Tension (top chord) force $=6.361$ Kips in Member \#7; Comb4 Max. Compr (Bottom chord) force $=6.363$ Kips in Member \#20; Comb4 Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## For Interior Vertical Member.

gravity load +1/2 of 1.0\% of Max. Top Chord Axial Force
Tension $=\mathrm{g}+1 / 2\left(1 \%{ }^{*}\right.$ Pep $)=$
Tension $=0.425$ Kips $+0.5(0.01 * 3.070100$ Kips $)=0.440$ Kips
Max. Tension $=0.440 \mathrm{Kips} ;($ Change $)$
Compresion $=g+1 / 2(1 \% *$ Pep $)=$
Compresion $=0.761$ Kips $+0.5\left(0.01^{*} 15.789752\right.$ Kips $)=0.796$ Kips
Max. Compresion = 0.840 Kips;(Change)

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(1.849^{*} 12\right) / 0.125=177.500$
S.R. $y=\left(L^{*} 12\right) / r y=\left(1.849^{*} 12\right) / 0.125=177.500$
S.R. $z=\left(L^{*} 12\right) / r z=\left(1.849^{*} 12\right) / 0.125=177.500$

Control $=177.500$
Comp. Ratio $=$ Control/200 $=177.50 / 200=0.89$
Comp. Status: $0.89<1.00 \ll--$ OK
Tens. Ratio $=$ Control/ $240=177.50 / 240=0.74$
Tens. Status: $0.74<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 1.85^{*} 12\right) / 0.125=133.125$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.900^{*} 1.85^{*} 12\right) / 0.125=159.750$

SLRgov=159.75
Fy=50.00 ksi;
Area=0.20 in^2;Comp=0.84 kips; fa=Comp/Area=4.28 ksi
$\mathrm{Fe}=11.22 \mathrm{ksi}$; Fcr=9.84 ksi
Fcr $=9.84 \mathrm{ksi} ;$ Fa=0.6Fcr= $=5.90 \mathrm{ksi}$
IRc=fa/Fa=4.279/5.902=0.730
Comp. Status: 0.73 <= 1.00 <<-- OK

## CHECK TENSION (Eq. 4.2-2)

$\mathrm{ft}=$ Tens $\times$ factor/Area $=(0.440 \times 1.000) / 0.196=2.242 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=2.24 / 30.00=0.07$
Status: $0.07<1.00 \ll-$ OK

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force $=0.840$; weld size $=1 / 8^{\prime \prime}$
Lenght weld $=$ Force $\times$ OMEGAw/(2 * Fnw x tef )
Lenght weld $=0.840 \times 2.0 /(2 \times 42.000 .170)=0.118 \mathrm{in}$.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]
CHECK ECCENTRICITY (4.5.4)
Woking point in both end: 0.0in. OK
This is important to fabrication.

## DESIGN MEMBER

INPUT FORM ( ASD ) Revision SJI 100-2020
Member Number = 49
Serial $=\mathrm{K}$
Member name = Right end web member
Type = Single(2)
Section = 0
Designation $=\mathrm{R} 7 / 8 ; \mathrm{A}=0.601^{\wedge} 2 ; \mathrm{Fy}=50 \mathrm{ksi}$
Reinforcement = NA;
Span design = 260.00 in
Lenght Member $=2^{\prime}-109 / 16^{\prime \prime}=2.880 \mathrm{ft}$. $=34.56 \mathrm{in}$.
Tension \& Compression Factor Design $=1.000$
Max. Code Check Ratio $=1.00$
$\Omega$ (Omega) $=1.67=1 / 1.67=0.6$; Spec. Section 4.2.3 Eq. 4.2
Omega Welding $=2.00$ Ref. SJI Spec 4.2.3.4
Min. Thicknees Material $=1 / 8^{\prime \prime}=0.125 \mathrm{in}$.
Weld Size(tw) $=1 / 8^{\prime \prime}=0.215 \mathrm{in} .=3.440$ (Weld Throat for Rod)

## EFFECTIVE SLENDERNESS RATIOS TABLE 4.3-1

Maximun Slenderness Ratio (all = allowable)
For Compression member Slenderness Ratio(L/r)all = 200
For Tension member Slenderness Ratio(L/r)all = 240

## Data Member

Yield Stress: Fy=50 ksi
Modulus of Elasticity: E=29000 ksi
Area $=0.601$ in^2; $\mathrm{k}=0.318$ inches
Inertia $x=0.029$ in $^{\wedge} 4, \mathrm{ly}=0.313 \mathrm{in}^{\wedge} 4$
$r x=0.22 \mathrm{in} ; r y=0.22 \mathrm{in} ; \mathrm{y}=0.438 \mathrm{in}$
$\mathrm{rz}=0.219 \mathrm{in} ;$ Qs $=1.000$
Spacing between chord angles $=0.500$ in $=1 / 2^{\prime \prime}$
Combination; [SW=Self Weight; F=Factor]
COMB1 $=1.00 x D L+1.00 x L L+[S W ~ F=1.00]$
COMB2 $=$ Not Active or Null this Combination
COMB3 $=1.00 x L L+[$ SW F=1.00]
COMB4 $=0.60 \times D L+1.00 \times U P+[S W F=0.60]$

## Summary Combination Maximun Results

| COMB | T. FORCE <br> Kips | C. FORCE <br> Kips | SHEAR <br> Kips | MOM(Mi) <br> K-in | MOM(Me) <br> K-in |
| :--- | :--- | :--- | :--- | :--- | :--- |
| COMB1 | 7.932 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB3 | 6.583 | 0.000 | 0.000 | 0.000 | 0.000 |
| COMB4 | 0.000 | 3.540 | 0.000 | 0.000 | 0.000 |

Max. Local Shear $(\mathrm{V})=0.000000$ Kips; Location in COMB4
Max. Moment $(\mathrm{Me})=0.000000 \mathrm{~K}$-ft; Location in COMB4
Max. Moment $(\mathrm{Mi})=0.000000$ K-ft; Location in COMB4
Max. Tension = 7.932 Kips; Location in COMB1
Max. Compresion = 3.540 Kips; Location in COMB4
Original COMPRESION = YES (Use for internal information only)

## Location of Reaction of Force

Max. Reation (Comb. \#4)= -1.894 Kips-Use in web member w/Tension
Max. Reation (Comb. \#1) $=4.207$ Kips-Use in web member w/Compr.

## For Web Member Check 25\% of Reaction.

Comp=3.540; Tens=7.932; seno = 0.498; Max. 25\% Reaction
Vertical Shear(Tens) $=3.949$; Vertical Shear(Comp) $=1.762$
Max. Tension = 7.932 Kips; ( Not Change)
Max. Compresion = 3.540 Kips; ( Not Change)

## Slenderness Ratio

k For Calculation Fcr per Table 4.3-1
(Comp.) $\mathrm{Kx}=0.75$; $\mathrm{Ky}=0.80$; Kz=0.00

## Max. Axial Force Top \& Bottom Chord Local

Max. Compr (top chord) force $=15.790$ Kips in Member \#7; Comb1
Max. Tension (top chord) force = 6.361 Kips in Member \#7; Comb4
Max. Compr (Bottom chord) force = 6.363 Kips in Member \#20; Comb4
Max. Tension (Bottom chord) force $=15.790$ Kips in Member \#20; Comb1

## CHECK SLENDERNESS RATIOS

S.R. $x=\left(L^{*} 12\right) / r x=\left(2.880^{*} 12\right) / 0.219=158.000$
S.R. $y=\left(L^{*} 12\right) / r y=\left(2.880^{*} 12\right) / 0.219=158.000$
S.R. $z=\left(L^{*} 12\right) / r z=(2.880 * 12) / 0.219=158.000$

Control $=158.000$
Comp. Ratio $=$ Control $/ 200=158.00 / 200=0.79$
Comp. Status: $0.79<1.00 \ll-$ OK
Tens. Ratio $=$ Control $/ 240=158.00 / 240=0.66$
Tens. Status: $0.66<1.00 \ll-$ OK

## CHECK COMPRESSION (4.2-4)

Shim, fillers or ties: NOT
S.R. $x=\left(K x^{*} L^{*} 12\right) / r x=\left(0.750^{*} 2.88^{*} 12\right) / 0.219=118.500$
S.R. $y=\left(k y^{*} L^{*} 12\right) / r y=\left(0.800^{*} 2.88^{*} 12\right) / 0.219=126.400$

SLRgov=126.40
Fy $=50.00 \mathrm{ksi}$;
Area=0.60 in^2;Comp=3.54 kips; fa=Comp/Area=5.89 ksi
Fe=17.91 ksi; Fcr=15.71 ksi
Fcr=15.71 ksi; Fa=0.6Fcr= 9.43 ksi
IRc=fa/Fa=5.887/9.427=0.620
Comp. Status: $0.62<=1.00 \ll-$ OK
CHECK TENSION (Eq. 4.2-2)
$\mathrm{ft}=$ Tens $\times$ factor/Area $=(7.932 \times 1.000) / 0.601=13.191 \mathrm{ksi}$
$\mathrm{Ft}=0.6(\mathrm{Fy})=0.6 * 50.000=30.000 \mathrm{ksi}$
Ratio $=\mathrm{ft} / \mathrm{Ft}=13.19 / 30.00=0.44$
Status: $0.44<=0.90^{* * *} \ll--$ OK
***Refer to Section 1.2B for applicationb of and the requirement for the use of the 0.90 Stress Interaction
Ratio for design check of first end web.

## WELDING WEB MEMBER

Strength of E70XX electrodes: Fexx=70 ksi
Force=7.932; weld size = 1/8"
Lenght weld $=$ Force $\times \mathrm{OMEGAw} /(2$ * Fnw $\times$ tef $)$
Lenght weld $=7.932 \times 2.0 /(2 \times 42.000 .215)=0.878$ in.
Use: $1 / 8^{\prime \prime} ; 2$ inches Both end (total lenght) [But use 1 in . Min. each leg of each end]

## CHECK ECCENTRICITY (4.5.4)

Woking point in both end: 0.0in. OK
This is important to fabrication.

